## Traffic Impact Study Riverwoods Reserve

Riverwoods, Illinois


Prepared For:
Lexington
Homes


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## 1. Introduction

This report summarizes the methodologies, results, and findings of a traffic impact study conducted by Kenig, Lindgren, O’Hara, Aboona, Inc. (KLOA, Inc.) for Riverwoods Reserve, a proposed townhome development to be located in Riverwoods, Illinois. The site, which contains the Federal Life Companies office building, is located on the north side of Deerfield Road (Lake County Highway A47) approximately 450 feet east of its intersection with Milwaukee Avenue (Illinois Route 21/ U.S. Route 45). As proposed, the site will be redeveloped with a townhome development with 69 units in 12 buildings. Access to the development will be provided via two proposed access roads on Deerfield Road that will replace the two existing access drives that serve the site.

The purpose of this study was to examine background traffic conditions, assess the impact that the proposed townhome development will have on traffic conditions in the area, and determine if any roadway or access improvements are necessary to accommodate traffic generated by the proposed development. Figure 1 shows the location of the site in relation to the area roadway system. Figure 2 shows an aerial view of the site. The sections of this report present the following:

- Existing roadway conditions
- A description of the proposed townhome development
- Directional distribution of the townhome development traffic
- Vehicle trip generation for the townhome development
- Future traffic conditions including the proposed Thorntons fuel center, the interim roadway improvements, the planned LCDOT Deerfield Road improvements, and access to the proposed townhome development
- Traffic analyses for the weekday morning and weekday evening peak hours
- Recommendations with respect to adequacy of the site access and adjacent roadway system

Traffic capacity analyses were conducted for the weekday morning and weekday evening for the following conditions:

1. Year 2021 - Base Conditions - Analyzes the capacity of the existing roadway system using peak hour traffic volumes adjusted to represent pre-pandemic Year 2021 traffic conditions.
2. Year 2024 - No-Build Conditions - Analyzes the capacity of the existing roadway system using Year 2021 base traffic volumes increased by an ambient area growth factor not attributable to any particular development as well as the traffic expected to be generated by the proposed Thorntons fuel center.
3. Year 2024 - Total Projected Conditions - Analyzes the capacity of the future roadway system assuming the projected traffic volumes that include Year 2024 no build traffic volumes and the traffic estimated to be generated by the proposed townhome development.
4. Year 2024 - Total Projected Conditions with Deerfield Road Improvements - Analyzes the capacity of the future roadway system assuming the 2024 total projected traffic volumes accounting for Lake County's planned roadway improvements to Deerfield Road.



Aerial View of Site
Figure 2

## 2. Existing Conditions

Existing transportation conditions in the vicinity of the site were documented based on field visits conducted by KLOA, Inc. in order to obtain a database for projecting future conditions. The following provides a description of the geographical location of the site, physical characteristics of the area roadway system including lane usage and traffic control devices, and existing peak hour traffic volumes.

## Site Location

The site, which contains the Federal Life Companies office building, is bounded by the Meadowlake residential subdivision to the north, a single-family home to the east, Deerfield Road to the south, and Colonial Court to the west. Existing land uses in the vicinity of the site are primarily commercial and residential and include CubeSmart self-storage and Brentwood North health care center to the south and Woodman's Food Market and the Shops of Buffalo Grove to the west.

## Existing Roadway System Characteristics

The characteristics of the existing roadways near the proposed townhome development are described below and illustrated in Figure 3.

Milwaukee Avenue (Illinois Route 21, U.S. Route 45) is a north-south, principal arterial roadway that provides two through lanes in each direction. At its signalized intersection with Deerfield Road, Milwaukee Avenue provides dual left turn lanes, a through lane, and a shared through/rightturn lane on the northbound approach and dual left-turn lanes, two through lanes, and an exclusive right-turn lane on the southbound approach. Milwaukee Avenue is under the jurisdiction of the Illinois Department of Transportation (IDOT), is classified as a Strategic Regional Arterial (SRA) route, carries an annual average daily traffic (AADT) volume of 35,600 vehicles north of Deerfield Road and 36,200 vehicles south of Deerfield Road (IDOT 2019), and has a posted speed limit of 40 miles per hour (mph).

Deerfield Road/Deerfield Parkway (Lake County Highway A47) is an east-west, minor arterial roadway that provides one through lane in each direction east of Milwaukee Avenue and two eastbound lanes and three westbound lanes west of Milwaukee Avenue. At its signalized intersection with Milwaukee Avenue, Deerfield Road provides an exclusive left-turn lane, two through lanes, and an exclusive right-turn lane on the eastbound approach and exclusive left-turn lane, a through lane, and a shared through/right-turn lane on the westbound approach. At its unsignalized intersections with the Colonial Court access drive, Federal Life Companies access drives, CubeSmart access road, and Brentwood North access drives, Deerfield Road provides no exclusive turn lanes. Deerfield Road is under the jurisdiction of the Lake County Division of Transportation (LCDOT) and carries an AADT volume of 15,600 vehicles west of Milwaukee Avenue and 17,400 vehicles east of Milwaukee Avenue (IDOT 2019).


Chicory Lane is a local roadway that extends north from Deerfield Road where it turns west and terminates at Milwaukee Avenue. Chicory Lane provides one lane in each direction and serves as the access road for the Meadowlake residential subdivision. At its unsignalized intersection with Deerfield Road, Chicory Lane provides a shared left-turn/right-turn lane and is under stop sign control. Chicory Lane is under the jurisdiction of the Village of Riverwoods.

## Existing Traffic Volumes

In order to determine current traffic conditions within the study area, KLOA, Inc. conducted peak period traffic counts utilizing Miovision Scout Collection Units at the following intersections:

Tuesday, May 11, 2021:

- Milwaukee Avenue with Deerfield Road
- Deerfield Road with the Colonial Court access drive
- Deerfield Road with the CubeSmart access road and the Federal Life Companies west access road
- Deerfield Road with the west Brentwood North access drive

Tuesday, November 30, 2021:

- Deerfield Road with Chicory Lane

The traffic counts were conducted during the weekday morning (7:00 A.M. to 9:00 A.M.) and weekday evening (4:00 P.M. to 6:00 P.M.) peak periods. The results of the traffic counts show that the peak hours of traffic generally occur between 7:30 A.M. and 8:30 A.M. during the weekday morning peak period and between 4:30 P.M. and 5:30 P.M. during the weekday evening peak period. Copies of the traffic count summary sheets are included in the Appendix.

Given the ongoing pandemic, the 2021 traffic volumes were compared to hourly counts conducted by IDOT on Milwaukee Avenue and Deerfield Road in 2019 and to the 2016 traffic volumes included in the IDS for the planned improvements at this intersection. The counts from the 2016 counts from the IDS were used, accounting for five years of growth, to provide for conservative and accurate analysis. The growth for the individual movements at the intersection were based on the growth rates included in the 2016 IDS. A copy of the IDS in included in the appendix. The Year 2021 base traffic volumes are illustrated in Figure 4.


## Crash Analysis

KLOA, Inc. obtained crash data ${ }^{1}$ from IDOT for the most recent available five years (2016 to 2020) for the intersections of Milwaukee Avenue with Deerfield Road, Deerfield Road with the access drives east of Milwaukee Avenue, and Deerfield Road with Chicory Lane. A review of the crash data indicated that no fatalities were reported at any of the intersections during the review period. Further, only five crashes were reported at the intersection of Deerfield Road with the access drives and only one crash was reported at the intersection of Deerfield Road with Chicory Lane. Table 1 summarizes the crash data for the intersection of Milwaukee Avenue with Deerfield Road.

Table 1
MILWAUKEE AVENUE WITH DEERFIELD ROAD - CRASH SUMMARY

| Year | Type of Crash Frequency |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Angle | Head On | Object | Rear End | Sideswipe | Turning | Other | Total |  |
| 2016 | 1 | 0 | 0 | 9 | 3 | 1 | 0 | 14 |  |
| 2017 | 1 | 1 | 1 | 9 | 2 | 12 | 0 | 26 |  |
| 2018 | 1 | 1 | 2 | 9 | 3 | 7 | 0 | 23 |  |
| 2019 | 2 | 0 | 1 | 11 | 1 | 4 | 0 | 19 |  |
| 2020 | $\underline{2}$ | $\underline{0}$ | $\underline{1}$ | $\underline{8}$ | $\underline{1}$ | $\underline{1}$ | $\underline{0}$ | $\underline{13}$ |  |
| Total | $\mathbf{7}$ | $\mathbf{2}$ | $\mathbf{5}$ | $\mathbf{4 6}$ | $\mathbf{1 0}$ | $\mathbf{2 5}$ | $\mathbf{0}$ | $\mathbf{9 5}$ |  |
| Average | $\mathbf{1 . 4}$ | $<\mathbf{1 . 0}$ | $\mathbf{1 . 0}$ | $\mathbf{9 . 2}$ | $\mathbf{2 . 0}$ | $\mathbf{5 . 0}$ | -- | $\mathbf{1 9}$ |  |

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## 3. Traffic Characteristics of the Proposed Development

In order to properly evaluate future traffic conditions in the surrounding area, it was necessary to determine the traffic characteristics of the proposed townhome development, including the directional distribution and volumes of traffic that it will generate.

## Interim Roadway Improvements

As part of the proposed Thorntons fuel center that will be located in the southeast quadrant of the intersection of Deerfield Road with Milwaukee Avenue, Deerfield Road will be improved as follows:

- The existing right-in/right-out access drive on Deerfield Avenue serving the CubeSmart access road, which will serve the proposed fuel center in addition to CubeSmart, will be modified to allow for inbound and outbound left-turn movements. Further, the access road will be widened to provide two outbound lanes striped for an exclusive left-turn lane and a shared through/right-turn lane.
- The west Brentwood North access drive will be eliminated and a connection from the Brentwood North parking lot to the CubeSmart Access Road will be provided.
- Deerfield Road will be widened at its intersection with the CubeSmart access road and the west site access road to provide exclusive westbound and eastbound left turn lanes. Further, a westbound right-turn lane serving the CubeSmart access road will be provided.
- A right-in/right-out access serving the fuel center will be provided on the south side of Deerfield Road approximately 380 feet east of Milwaukee Avenue aligned opposite the Colonial Court access drive. An exclusive right-turn lane will be provided on Deerfield Road serving this access drive.


## Proposed Development Plan

As proposed, the site will be developed with Riverwoods Reserve, a townhome development with 69 townhome units in 12 buildings. Access to the development will be provided via the following:

- A proposed full movement access road on the north side of Deerfield Road approximately 820 feet east of Milwaukee Avenue. This access road will replace the existing Federal Life Companies access road at this location and will also be aligned opposite the CubeSmart access road. This access road should provide one inbound lane and two outbounds striped to provide an exclusive left-turn lane and a shared through/right-turn lane. Outbound movements will be under stop sign control. As previously mentioned, as part of the Thorntons fuel center roadway improvements, an exclusive eastbound left-turn lane will be provided on Deerfield Road serving this access road. The left-turn lane will continue to be provided as part of the planned LCDOT Deerfield Road improvements. This turn lane will provide 117 feet of storage and a 270 -foot taper.
- A proposed full movement access road on the north side of Deerfield Road approximately 1,160 feet east of Milwaukee Avenue. This access road will replace the existing Federal Life Companies access drive at this location. This access road will provide one inbound lane and one outbound lane with outbound movements under stop sign control. With the completion of the planned LCDOT Deerfield Road improvements, this access road will be restricted to right-turn only movements via striping, signage, and a raised triangular median.

It is important to note that a future connection will be provided between the proposed development and the Colonial Court development that borders the site to the west. However, since the timing of this connection is not known at this time, it was not included in the study. A site plan depicting the proposed townhome development layout is included in the Appendix.

## Directional Distribution

The directions from which residents of the proposed townhome development will approach and depart the site were estimated based on existing travel patterns, as determined from the traffic counts. Figure 5 illustrates the directional distribution of the townhome development-generated traffic.

## Peak Hour Traffic Volumes

The number of peak hour trips estimated to be generated by the proposed townhome development was based on vehicle trip generation rates contained in Trip Generation Manual, 11th Edition, published by the Institute of Transportation Engineers (ITE). The "Single Family Attached Housing" (Land-Use Code 215) rates were used for the proposed development. Table 2 summarizes the trips projected to be generated by the proposed townhome development.

Table 2
PROJECTED SITE-GENERATED TRAFFIC VOLUMES

| $\begin{gathered} \hline \text { ITE } \\ \text { Land- } \end{gathered}$ | Land Use/Size | Weekday Morning Peak Hour |  |  | Weekday Evening Peak Hour |  |  | Daily Traffic |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Code |  | In | Out | Total | In | Out | Total | In | Out |
| 215 | Single Family Attached Housing (69 Units) | 9 | 21 | 30 | 21 | 16 | 37 | 238 | 238 |



## Trip Generation Comparison

The site is currently occupied by the approximately 48,896 square-foot Federal Life Companies office building. Table 3 provides a comparison of the traffic estimated to be generated by the proposed development compared to the traffic that would have been generated by the office building based on ITE trip generation rates. As can be seen, the proposed development will generate significantly less traffic than the office building would generate at full occupancy.

Table 3
TRIP GENERATION COMPARISON

| ITE <br> Land- | Type/Size | Weekday Morning Peak Hour |  |  | Weekday Evening Peak Hour |  |  | Daily <br> Trips |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Code |  | In | Out | Total | In | Out | Total | In | Out |
| 215 | Proposed Development | 9 | 21 | 30 | 21 | 16 | 37 | 238 | 238 |
| 710 | General Office (48,896 s.f.) | 79 | 11 | 90 | 16 | 76 | 92 | 312 | 312 |
|  | Difference | -70 | +10 | -60 | +5 | -60 | -55 | -74 | -74 |

## 4. Projected Traffic Conditions

The total projected traffic volumes include the base traffic volumes, increase in background traffic due to growth, and the traffic estimated to be generated by the proposed townhome development.

## Townhome Development Traffic Assignment

The estimated weekday morning and evening peak hour traffic volumes that will be generated by the proposed townhome development were assigned to the roadway system in accordance with the previously described directional distribution (Figure 5). Figure 6 illustrates the traffic assignment of the new development trips.

## Background (No-Build) Traffic Volumes

In addition to the traffic to be generated by the proposed development, the study also considered the following additional regional growth and other developments proposed in the area:

- The base traffic volumes (Figure 4) were increased by a regional growth factor to account for the increase in existing traffic related to regional growth in the area (i.e., not attributable to any particular planned development). Per Lake County's Highway Access and Use Ordinance, the existing volumes should be increased by three percent for two years. However, as the planned LCDOT Deerfield Road improvements are not expected to be completed until 2024, the background traffic volumes were increased for three years for a total of nine percent.
- The proposed Thorntons fuel center to be built in the southeast quadrant of the intersection of Milwaukee Avenue with Deerfield Road. As proposed, the fuel center will provide 20 passenger vehicle fueling positions and a convenience store. As previously mentioned, interim roadway improvements will be provided on Deerfield Road as part of this development. Access to the proposed fuel center will be provided via the CubeSmart access road and via the proposed right-in/right-out access drive on Deerfield Road. The volume of traffic estimated to be generated by this development was based on the KLOA, Inc. traffic impact study dated July 16, 2021.

The Year 2024 no-build traffic volumes, which include the Year 2021 base traffic volumes increased by the ambient growth factor as well as the traffic estimated to be generated by the proposed Thorntons fuel center, are illustrated in Figure 7.

## Total Projected Traffic Volumes

The development-generated traffic (Figure 6) was added to the projected Year 2024 no-build traffic volumes (Figure 7) to determine the projected Year 2024 total traffic volumes as illustrated in Figure 8.




## Deerfield Road Planned Improvements

LCDOT is planning to improve Deerfield Road for two miles between Milwaukee Avenue and Saunders Road and is currently in Phase II planning for the project. The following improvements are planned for the study area:

- The intersection of Milwaukee Avenue with Deerfield Road will be improved and will provide dual left-turn lanes, two through lanes, and an exclusive right-turn lane on the eastbound approach, dual left-turn lanes, three through lanes, and an exclusive right-turn lane on the westbound approach, and dual left-turn lanes, two through lanes, and an exclusive right-turn lane on the northbound and southbound approaches. In addition, highvisibility crosswalks and pedestrian signals will be provided on all legs.
- Deerfield Road will be widened to provide two eastbound lanes and three westbound lanes between Milwaukee Avenue and the east site access road (approximately 1,200 feet east of Milwaukee Avenue).
- East of the east site access road, Deerfield Road will be widened to provide two westbound lanes and one eastbound lane divided by a two-way left-turn lane.
- The east site access road will be restricted to right-turn movements only.
- The Colonial Court access drive on Deerfield Road will be restricted to right-turn only movements via the barrier median on Deerfield Road.
- A multi-use path will be provided on the south side of Deerfield Road.

The improvements are expected to be completed by 2024. It should be noted that, as part of the road improvement project, the left-turn lanes serving the combined CubeSmart access road and the west site access road will be maintained.

Figure 9 illustrates the future roadway characteristics with the completion of the planned LCDOT improvements as well as the completion of the proposed Thorntons fuel center development.

With the provision of these improvements and the restriction of the east site access road to rightturn only, the estimated development generated traffic assignment will be modified as illustrated in Figure 10. Figure 11 illustrates the projected Year 2024 total traffic volumes with the completion of the roadway improvements.




## 5. Traffic Analysis and Recommendations

The following provides an evaluation conducted for the weekday morning and weekday evening peak hours. The analysis includes conducting capacity analyses to determine how well the roadway system and access roads are projected to operate and whether any roadway improvements or modifications are required.

## Traffic Analyses

Roadway and adjacent or nearby intersection analyses were performed for the weekday morning and weekday evening peak hours for the projected Year 2021 base, Year 2024 no-build, and Year 2024 total projected, and Year 2024 total projected with LCDOT roadway improvements traffic volumes.

The traffic analyses were performed using the methodologies outlined in the Transportation Research Board's Highway Capacity Manual (HCM), 6 ${ }^{\text {th }}$ Edition and analyzed using Synchro/SimTraffic 11 software. The analysis for the traffic signal-controlled intersections were performed using actual cycle lengths, phasings and offsets to determine the average overall vehicle delay and levels of service.

The analyses for the unsignalized intersections determine the average control delay to vehicles at an intersection. Control delay is the elapsed time from a vehicle joining the queue at a stop sign (includes the time required to decelerate to a stop) until its departure from the stop sign and resumption of free flow speed. The methodology analyzes each intersection approach controlled by a stop sign and considers traffic volumes on all approaches and lane characteristics.

The ability of an intersection to accommodate traffic flow is expressed in terms of level of service, which is assigned a letter from A to F based on the average control delay experienced by vehicles passing through the intersection. The Highway Capacity Manual definitions for levels of service and the corresponding control delay for signalized intersections and unsignalized intersections are included in the Appendix of this report.

Summaries of the traffic analysis results showing the level of service and overall intersection delay (measured in seconds) for the Year 2021 base, Year 2024 no-build, Year 2024 total projected, and Year 2024 total projected with LCDOT roadway improvements conditions are presented in Tables 4 through 8. A discussion of each intersection follows. Summary sheets for the capacity analyses are included in the Appendix.

Table 4
CAPACITY ANALYSIS RESULTS - MILWAUKEE AVENUE WITH DEERFIELD ROAD- SIGNALIZED

|  | Peak Hour |  | stbou |  |  | stbou |  |  | thbo |  |  | thbo |  | Overall |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | L | T | R | L | T | R | L | T | R | L | T | R |  |
|  | Weekday Morning Peak Hour | $\begin{gathered} \hline \mathrm{C} \\ 34.2 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 53.3 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 35.6 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 35.5 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { D } \\ 38.0 \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline \mathrm{E} \\ 61.9 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 53.4 \\ \hline \end{gathered}$ |  | $\begin{gathered} \mathrm{E} \\ 63.1 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 30.3 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 0.8 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ 44.7 \end{gathered}$ |
|  |  | D-44.2 |  |  | D-37.8 |  |  | D-54.8 |  |  | D-39.1 |  |  |  |
|  | Weekday Evening Peak Hour | $\begin{gathered} \hline \mathrm{D} \\ 37.4 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 40.1 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{B} \\ 15.7 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 28.4 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{F} \\ 99+ \end{gathered}$ |  | $\begin{gathered} \hline \mathrm{E} \\ 69.0 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 69.7 \end{gathered}$ |  | $\begin{gathered} \hline \mathrm{E} \\ 78.8 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{E} \\ 69.9 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 4.2 \end{gathered}$ | $\begin{gathered} \text { E } \\ 77.9 \end{gathered}$ |
|  |  | C-28.7 |  |  | F - 99+ |  |  | E-69.5 |  |  | E-69.6 |  |  |  |
|  | Weekday Morning Peak Hour | $\begin{gathered} \text { C } \\ 34.5 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{E} \\ 58.6 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 44.8 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 41.9 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 40.7 \\ \hline \end{gathered}$ |  | $\begin{gathered} \mathrm{E} \\ 63.8 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{F} \\ 99+ \end{gathered}$ |  | $\begin{gathered} \hline \mathrm{E} \\ 69.9 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 34.5 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 1.2 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 62.8 \end{gathered}$ |
|  |  | D-51.1 |  |  | D - 40.8 |  |  | F - 99+ |  |  | D-44.6 |  |  |  |
|  | Weekday Evening Peak Hour | $\begin{gathered} \hline \mathrm{D} \\ 39.0 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 41.2 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{B} \\ 19.6 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { C } \\ 29.9 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{F} \\ 99+ \end{gathered}$ |  | $\begin{gathered} \mathrm{E} \\ 76.3 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{F} \\ 99+ \end{gathered}$ |  | $\begin{gathered} \hline \mathrm{F} \\ 99+ \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{F} \\ 99+ \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{A} \\ 4.8 \end{gathered}$ | $\underset{\text { F }}{\mathrm{F}}$ |
|  |  | C-31.3 |  |  | F-99+ |  |  | F-99+ |  |  | F-99.9 |  |  |  |
|  | Weekday Morning Peak Hour | $\begin{gathered} \hline \mathrm{C} \\ 34.5 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{E} \\ 58.7 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 45.0 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 43.3 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ 41.9 \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline \mathrm{E} \\ 63.8 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{F} \\ 99+ \\ \hline \end{gathered}$ |  | $\begin{gathered} \hline \mathrm{E} \\ 70.3 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 34.6 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 1.2 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 63.5 \end{gathered}$ |
|  |  | D-51.3 |  |  | D-42.0 |  |  | F-99+ |  |  | D-44.7 |  |  |  |
|  | Weekday Evening | $\begin{gathered} \hline \mathrm{D} \\ 39.0 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{D} \\ 41.3 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { B } \\ 19.9 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{C} \\ 30.0 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{F} \\ 99+ \end{gathered}$ |  | $\begin{gathered} \mathrm{E} \\ 76.3 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \mathrm{F} \\ 99+ \end{gathered}$ |  | $\begin{gathered} \hline \mathrm{F} \\ 99+ \end{gathered}$ | $\begin{gathered} \hline \mathrm{F} \\ 99+ \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 4.8 \end{gathered}$ | $\begin{gathered} \text { F } \\ 99+ \end{gathered}$ |
|  | Peak Hour | C-31.5 |  |  | F-99+ |  |  | F-99+ |  |  | F-99+ |  |  |  |
|  | Weekday Morning Peak Hour | $\begin{gathered} c \\ \text { C } \\ 27.0 \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ 53.5 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ 42.0 \\ \hline \end{gathered}$ | $\begin{gathered} \text { C } \\ 29.5 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { D } \\ 38.1 \end{gathered}$ | $\begin{gathered} \text { C } \\ 24.2 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 62.3 \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 80.6 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 6.5 \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 65.7 \end{gathered}$ | $\begin{gathered} \text { C } \\ 35.3 \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { A } \\ 1.1 \end{gathered}$ | $\begin{gathered} \text { D } \\ 50.2 \end{gathered}$ |
|  |  | D - 46.8 |  |  | C - 29.1 |  |  | E-71.1 |  |  | D-43.9 |  |  |  |
|  | Weekday Evening Peak Hour | $\begin{gathered} \mathrm{E} \\ 59.9 \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ 42.5 \end{gathered}$ | $\begin{gathered} \text { C } \\ 24.3 \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 60.8 \end{gathered}$ | $\begin{gathered} \text { D } \\ 48.2 \end{gathered}$ | $\begin{gathered} \text { C } \\ 24.6 \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 74.5 \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 66.8 \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ 1.8 \end{gathered}$ | $\begin{gathered} F \\ 95.4 \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 76.4 \end{gathered}$ | $\begin{gathered} \text { A } \\ 3.7 \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ 61.9 \end{gathered}$ |
|  |  | D - 36.9 |  |  | D - 43.1 |  |  | E-66.9 |  |  | E-78.6 |  |  |  |
| 1- Includes Interim Roadway Improvements   <br> L Includes <br> LCDOT Leter denotes Level of Service <br> Delay is measured in seconds. L- Left TurnsR-Right Turns <br> T-Through |  |  |  |  |  |  |  | L - Left Turns R - Right Turns <br> T- Through |  |  |  |  |  |  |

Table 5
CAPACITY ANALYSIS RESULTS - EXISTING CONDITIONS - UNSIGNALIZED

| Intersection | Weekday Morning Peak Hour |  | Weekday Evening Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |
| Deerfield Road with the Colonial Court Access Drive |  |  |  |  |
| - Eastbound Left Turn | B | 11.1 | B | 11.0 |
| - Southbound Approach | C | 23.2 | D | 26.1 |
| Deerfield Road with the CubeSmart Access Drive and the West Federal Life Companies Access Drive |  |  |  |  |
| - Eastbound Left Turn | A | 9.9 | B | 11.1 |
| - Northbound Approach | C | 20.8 | B | 14.9 |
| - Southbound Approach | -- | -- | -- | -- |
| Deerfield Road with the West Brentwood North Access Drive |  |  |  |  |
| - Westbound Left Turn | B | 11.2 | A | 9.2 |
| - Northbound Approach | F | 55.4 | F | 59.5 |
| Deerfield Road with Chicory Lane |  |  |  |  |
| - Eastbound Left Turn | A | 9.7 | B | 12.0 |
| - Southbound Approach | F | 56.8 | F | 55.6 |
| LOS $=$ Level of Service $\quad$ Delay is measured in seconds. |  |  |  |  |

Table 6


| Deerfield Road with the Colonial Court Access Drive and the Thorntons Access Drive |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| - Eastbound Left Turn | B | 11.7 | B | 11.7 |
| - Northbound Approach | B | 13.7 | B | 11.2 |
| - Southbound Approach | D | 36.3 | E | 45.4 |
| Deerfield Road with the CubeSmart Access Drive and the West Federal Life Companies Access Drive |  |  |  |  |
| - Eastbound Left Turn | B | 10.2 | B | 11.5 |
| - Westbound Left Turn | B | 12.2 | A | 9.7 |
| - Northbound Left Turn | F | 53.3 | F | 55.9 |
| - Northbound Right Turn | C | 23.7 | C | 16.2 |
| - Southbound Approach | -- | -- | -- | -- |
| Deerfield Road with Chicory Lane |  |  |  |  |
| - Eastbound Left Turn | A | 10.1 | B | 12.9 |
| - Southbound Approach | F | 80.3 | F | 78.0 |
| Includes interim roadway improvements | LOS = Level of Service | Delay is measured in seconds |  |  |

Table 7
CAPACITY ANALYSIS RESULTS - TOTAL PROJECTED CONDITIONS UNSIGNALIZED

| Intersection | Weekday Morning <br> Peak Hour |  | Weekday Evening <br> Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |


| Deerfield Road with the Colonial Court Access Drive and the Thorntons Access Drive |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| - | Eastbound Left Turn | B | 11.8 | B | 11.8 |
| - | Northbound Approach | B | 13.8 | B | 11.3 |
| - Southbound Approach | E | 37.2 | E | 46.3 |  |

Deerfield Road with the CubeSmart Access Drive and the West Site Access Road

| - Eastbound Left Turn | B | 10.3 | B | 11.6 |
| :--- | :--- | :--- | :--- | :---: |
| - Westbound Left Turn | B | 12.2 | A | 9.7 |
| - Northbound Left Turn | F | 55.3 | F | 64.6 |
| - Northbound Right Turn | C | 23.8 | C | 16.3 |
| - Southbound Left Turn | E | 41.8 | E | 35.8 |
| - Southbound Right Turn | C | 17.9 | C | 23.1 |

Deerfield Road with the East Site Access Road

| • Eastbound Left Turn | B | 10.0 | B | 11.6 |
| :---: | :---: | :---: | :---: | :---: |
| • Southbound Approach | E | 48.1 | E | 38.1 |
| Deerfield Road with Chicory Lane <br> $\bullet$ |  |  |  |  |
| E Eastbound Left Turn | Bouthbound Approach | F | 10.1 | B |
| Includes interim roadway improvements | LOS = Level of Service | 81.8 | F | Delay is measured in seconds. |

Table 8
CAPACITY ANALYSIS RESULTS - TOTAL PROJECTED CONDITIONS WITH THE PLANNED LCDOT DEERFIELD ROAD IMPROVEMENTS - UNSIGNALIZED

| Intersection | Weekday Morning <br> Peak Hour |  | Weekday Evening <br> Peak Hour |  |
| :---: | :---: | :---: | :---: | :---: |
|  | LOS | Delay | LOS | Delay |

Deerfield Road with the Colonial Court Access Drive and the Thorntons Access Drive

| - Northbound Approach | B | 13.8 | B | 11.4 |
| :---: | :---: | :---: | :---: | :---: |
| - Southbound Approach | B | 13.1 | C | 15.8 |


| Deerfield Road with the CubeSmart Access Drive and the West Site Access Road |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| • | Eastbound Left Turn | B | 14.1 | C |
| - | Westbound Left Turn | B | 12.2 | A |
| - | Northbound Left Turn | E | 43.6 | D |
| - | Northbound Right Turn | B | 13.9 | B |
| - | Southbound Left Turn | D | 33.0 | 12.1 |
| - | Southbound Right Turn | B | 13.4 | E |


| Deerfield Road with the East Site Access Road |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: |
| • Southbound Approach | B | 11.9 | B | 13.6 |
| Deerfield Road with Chicory Lane |  |  |  |  |
| • Eastbound Left Turn | B | 10.1 | B | 12.9 |
| • Southbound Approach | C | 24.9 | C | 24.9 |
| Includes LCDOT roadway <br> improvements | LOS = Level of Service |  | Delay is measured in seconds. |  |

## Discussion and Recommendations

The following summarizes how the intersections are projected to operate and identifies any roadway and traffic control improvements necessary to accommodate the townhome developmentgenerated traffic.

## Milwaukee Avenue with Deerfield Road

The results of the capacity analysis indicate that overall, this intersection currently operates at Level of Service (LOS) D during the weekday morning peak hour and at LOS E during the weekday evening peak hour. This level of service during the weekday evening peak hour is primarily due to the westbound approach which operates at LOS F. This delay is the result of the lack of a westbound right-turn lane and the fact that Milwaukee Avenue is an SRA route, and, as such, receives a majority of the green time. It should be noted that the northbound and southbound left turn movements operate at LOS E during the peak hours. This delay is due to the fact that these movements are restricted to protected turning movements only and receive a limited amount of green time.

Under Year 2024 no-build conditions, this intersection is projected to operate at LOS E during the weekday morning peak hour and LOS F during the weekday evening peak hour with increases in delay of approximately 18 and 28 seconds, respectively. This increase in delay is the result of increases to movements that operate at or over capacity under existing conditions. Under Year 2024 total projected conditions, this intersection is projected to continue to operate at LOS E during the weekday morning peak hour and LOS F during the weekday evening peak hour with increases in delay of approximately one to two seconds.

As previously mentioned, this intersection will be improved as part of LCDOT's planned improvements of Deerfield Road. With the completion of these improvements, this intersection will provide dual left turn lanes, two through lanes, and an exclusive right-turn lane on the eastbound approach, dual left turn lanes, three through lanes, and an exclusive right-turn lane on the westbound approach and dual left turn lanes, two through lanes, and an exclusive right-turn lane on the northbound and southbound approaches.

Under Year 2024 total projected conditions, assuming the completion of the planned LCDOT roadway improvements, this intersection is projected to operate at LOS D during the weekday morning peak hours and LOS E during the weekday evening peak hour with an increase in delay of approximately six seconds during the weekday morning peak hour and a decrease in delay during the weekday evening peak hour when compared to existing conditions. Further, all approaches are projected to operate at LOS E or better during both peak hours. In addition, westbound queues from this intersection are only projected to extend up to 265 feet and will not block the location of the site access roads.

Overall, the proposed development is projected to increase traffic at this intersection by less than one half of one percent and will have a minimal impact on this intersection. The planned improvements will significantly improve signal operations and alleviate existing capacity constraints.

The results of the capacity analysis indicate that all critical movements at this intersection operate at LOS D or better during the weekday morning and weekday evening peak hours. As part of the proposed Thorntons fuel center development, a right-in/right-out access drive serving the fuel center will be provided opposite this access drive. Under Year 2024 no build and Year 2024 total projected traffic conditions all critical movements are projected to operate at LOS E or better.

With the completion of the planned LCDOT Deerfield Road improvements, the Colonial Court access drive will be restricted to right-turn only movements by a barrier median on Deerfield Road. Under Year 2024 total projected conditions, assuming the completion of the planned roadway improvements, outbound movements from both access drives are projected to operate at LOS C or better. Overall, the proposed development will have a limited impact on the operations of this intersection and no geometric improvements or traffic control modifications will be required as a result of the construction of the proposed townhome development.

Deerfield Road with the CubeSmart Access Drive and the Federal Life Companies West Access Drive/West Site Access Road

The results of the capacity analysis indicate that the northbound and southbound approaches at this intersection currently operates at LOS C or better during the weekday morning and weekday evening peak hours and eastbound left-turn movements operate at LOS B or better.

As part of the proposed Thorntons fuel center development, the CubeSmart access road will be modified to allow left-turn movements and improved to provide two outbound lanes. Further, an eastbound left-turn lane, an eastbound right-turn lane, and a westbound left-turn lane will be provided at this intersection. Under Year 2024 no-build traffic conditions, all critical movements are projected to operate at LOS C or better with the exception of the northbound left-turn movement which is projected to operate at LOS F during the peak hours. This delay is typical and expected at the unsignalized intersection of an access road with an arterial roadway. Further, this movement is projected to operate with a volume to capacity ( $\mathrm{v} / \mathrm{c}$ ) ratio of less than one and $95^{\text {th }}$ percentile queues of approximately two vehicles indicating that vehicles will be able to exit.

As proposed, a full movement access road will be provided on the north side of Deerfield Road that will replace the existing Federal Life Companies west access road at this location. This access road should provide one inbound lane and two outbound lanes striped to provide an exclusive leftturn lane and a shared through/right-turn lane. Outbound movements will be under stop sign control. Under Year 2024 total projected conditions, outbound left-turn movements from the proposed access road are projected to operate at LOS E during the weekday morning and weekday evening peak hours. All other critical movements are projected to operate at LOS C or better with the exception of the northbound left turn movement which is projected to operate at LOS F during both peak hours.

With the completion of the planned LCDOT Deerfield Road improvements, this intersection will be widened to provide two eastbound through lanes and three westbound through lanes. Further, the eastbound right-turn lane will be removed. The eastbound and westbound left-turn lanes will be maintained. Under Year 2024 total projected conditions, assuming the completion of the planned roadway improvements, outbound left-turn movements from the proposed access road are projected to operate at LOS D during the weekday morning peak hour and LOS E during the weekday evening peak hour. Further, northbound left turn movements are projected to operate at LOS E or better during both peak hours and all other critical movements are projected to operate at LOS C or better during both peak hours.

When the projected traffic volumes at this access road are compared to the right-turn lane guidelines in Table 5.4 of Lake County's Highway Access and Use Ordinance Technical Reference Manual, a westbound right-turn lane on Deerfield Road will not be warranted serving this access road under any condition. It should be noted that based on Signal Warrant 3 (Peak Hour) included in the Federal Highway Administration’s Manual on Uniform Traffic Control Devices for Streets and Highways (MUTCD), 2009, a traffic signal will not be warranted at this intersection under any condition. As such, the intersection can adequately accommodate the development-generated traffic, and overall intersection operations will improve with the completion of the planned LCDOT Deerfield Road improvements.

## Deerfield Road with the Brentwood North Access Drive

The results of the capacity analysis indicate that the northbound approach at this intersection currently operates at LOS F during the weekday morning and weekday evening peak hours and is projected to continue to do so under Year 2024 no-build and total projected conditions. With the completion of the interim roadway improvements, this access drive will be combined with the CubeSmart access road which is projected to operate at an acceptable LOS.

## Deerfield Road with the Proposed East Site Access Road

As proposed, a full movement access road will be provided on the north side of Deerfield Road approximately 1,160 feet east of Milwaukee Avenue. This access road will replace the existing Federal Life Companies east access road at this location. This access road will provide one inbound lane and one outbound lane with outbound movements under stop sign control. The results of the capacity analysis indicate that under Year 2024 total projected conditions outbound movements from this access road will operate at LOS E during the weekday morning peak hour and weekday evening peak hours. Further, inbound left turn movements are projected to operate at LOS B or better during both peak hours.

With the completion of the planned LCDOT Deerfield Road improvements, this access road will be restricted to right-turn only movements via striping, signage, and a raised triangular median. Under Year 2024 total projected conditions, assuming the completion of the planned roadway improvements, outbound movements from the proposed access road are projected to operate at LOS B during both peak hours. When the projected traffic volumes at this access road are compared to the right-turn lane guidelines in Table 5.4 of Lake County's Highway Access and Use Ordinance Technical Reference Manual, a westbound right-turn lane on Deerfield Road will not be warranted serving this access road under any condition. As such, the proposed access road will adequately accommodate development-generated traffic.

## Deerfield Road with Chicory Lane

The results of the capacity analysis indicate that the southbound approach at this intersection currently operates at LOS F during the weekday morning and weekday evening peak hours and is projected to continue to do so under Year 2024 no-build and total projected conditions. With the completion of the planned LCDOT Deerfield Road improvements, Deerfield Road at this intersection will be improved to provide two westbound lanes, one eastbound lane, and a two-way left-turn lane. Under Year 2024 total projected conditions, assuming the completion of the planned LCDOT Deerfield Road improvements, outbound movements from Chicory Lane are projected to operate at LOS C during both peak hours. This decrease in delay is primarily the result of the provision of the two way-left-turn lane which will allow outbound left-turn vehicles to perform a two-part left turn. As such, the intersection can adequately accommodate the developmentgenerated traffic, and intersection operations will improve with the completion of the Deerfield Road improvements.

## 6. Conclusions

Based on the preceding analyses and recommendations, KLOA, Inc. has concluded as follows:

- The intersection of Milwaukee Avenue with Deerfield Road can adequately accommodate development generated traffic, especially with the construction of the planned LCDOT Deerfield Road improvements.
- Overall, the unsignalized intersections within the study area will be able to adequately accommodate the development-generated traffic, and operations at these intersections will improve with the completion of the planned LCDOT Deerfield Road improvements.
- The proposed access system will replace the existing access system on Deerfield Road and will not increase the total number of access points.
- The proposed access system will be able to accommodate the traffic projected to be generated by the proposed development regardless of the planned LCDOT Deerfield Road improvements. With the completion of the improvements, the access system will work at an improved LOS with reduced delay.
- An exclusive westbound right-turn lane will not be warranted on Deerfield Road serving either proposed access road.


## Appendix

Traffic Count Summary Sheets Milwaukee Avenue with Deerfield Road IDS Preliminary Site Plan ITE Trip Generation Worksheets Level of Service Criteria
Capacity Analysis Summary Sheets

## Traffic Count Summary Sheets

Rosemont, Illinois, United States 60018
(847)518-9990

Count Name: Deerfield Road with Milwaukee Avenue
Sitart Date: 05/08/2021
Page No: 1

Turning Movement Data

| Start Time | Deerfield Road Eastbound |  |  |  |  |  | Deerfield Road Westbound |  |  |  |  |  | Milwaukee Avenue Northbound |  |  |  |  |  | Milwaukee Avenue Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. | Int. Total |
| 11:30 AM | 0 | 46 | 92 | 68 | 0 | 206 | 0 | 32 | 81 | 38 | 0 | 151 | 0 | 68 | 209 | 10 | 0 | 287 | 1 | 48 | 214 | 0 | 0 | 263 | 907 |
| 11:45 AM | 0 | 38 | 59 | 55 | 0 | 152 | 0 | 17 | 70 | 46 | 0 | 133 | 0 | 68 | 228 | 17 | 0 | 313 | 0 | 41 | 198 | 0 | 0 | 239 | 837 |
| Hourly Total | 0 | 84 | 151 | 123 | 0 | 358 | 0 | 49 | 151 | 84 | 0 | 284 | 0 | 136 | 437 | 27 | 0 | 600 | 1 | 89 | 412 | 0 | 0 | 502 | 1744 |
| 12:00 PM | 0 | 32 | 97 | 89 | 0 | 218 | 0 | 32 | 75 | 57 | 0 | 164 | 0 | 81 | 219 | 20 | 0 | 320 | 2 | 56 | 200 | 0 | 0 | 258 | 960 |
| 12:15 PM | 0 | 31 | 74 | 71 | 0 | 176 | 0 | 11 | 76 | 37 | 0 | 124 | 0 | 91 | 243 | 12 | 0 | 346 | 0 | 44 | 222 | 0 | 0 | 266 | 912 |
| 12:30 PM | 0 | 43 | 94 | 82 | 0 | 219 | 0 | 23 | 74 | 32 | 0 | 129 | 1 | 67 | 193 | 12 | 0 | 273 | 0 | 57 | 208 | 0 | 0 | 265 | 886 |
| 12:45 PM | 0 | 44 | 68 | 77 | 0 | 189 | 0 | 16 | 64 | 48 | 0 | 128 | 0 | 71 | 252 | 13 | 0 | 336 | 0 | 52 | 242 | 0 | 0 | 294 | 947 |
| Hourly Total | 0 | 150 | 333 | 319 | 0 | 802 | 0 | 82 | 289 | 174 | 0 | 545 | 1 | 310 | 907 | 57 | 0 | 1275 | 2 | 209 | 872 | 0 | 0 | 1083 | 3705 |
| 1:00 PM | 0 | 44 | 81 | 83 | 0 | 208 | 0 | 40 | 87 | 53 | 0 | 180 | 0 | 60 | 222 | 10 | 0 | 292 | 1 | 46 | 206 | 0 | 0 | 253 | 933 |
| 1:15 PM | 0 | 36 | 63 | 63 | 0 | 162 | 0 | 19 | 71 | 39 | 0 | 129 | 0 | 67 | 219 | 22 | 0 | 308 | 0 | 58 | 234 | 0 | 0 | 292 | 891 |
| 1:30 PM | 0 | 41 | 94 | 80 | 0 | 215 | 0 | 15 | 77 | 68 | 0 | 160 | 1 | 79 | 185 | 20 | 2 | 285 | 0 | 47 | 184 | 0 | 0 | 231 | 891 |
| 1:45 PM | 0 | 34 | 56 | 61 | 0 | 151 | 0 | 28 | 63 | 38 | 0 | 129 | 0 | 74 | 220 | 11 | 0 | 305 | 0 | 56 | 231 | 0 | 0 | 287 | 872 |
| Hourly Total | 0 | 155 | 294 | 287 | 0 | 736 | 0 | 102 | 298 | 198 | 0 | 598 | 1 | 280 | 846 | 63 | 2 | 1190 | 1 | 207 | 855 | 0 | 0 | 1063 | 3587 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 7:00 AM | 0 | 17 | 93 | 42 | 0 | 152 | 0 | 4 | 32 | 38 | 0 | 74 | 0 | 36 | 159 | 14 | 0 | 209 | 0 | 33 | 121 | 0 | 0 | 154 | 589 |
| 7:15 AM | 0 | 16 | 107 | 44 | 0 | 167 | 0 | 4 | 50 | 67 | 0 | 121 | 0 | 38 | 179 | 25 | 0 | 242 | 0 | 38 | 177 | 0 | 0 | 215 | 745 |
| 7:30 AM | 0 | 24 | 102 | 64 | 0 | 190 | 0 | 13 | 45 | 51 | 0 | 109 | 0 | 41 | 222 | 15 | 0 | 278 | 0 | 49 | 170 | 0 | 0 | 219 | 796 |
| 7:45 AM | 0 | 27 | 120 | 65 | 0 | 212 | 0 | 5 | 45 | 70 | 0 | 120 | 0 | 60 | 233 | 19 | 0 | 312 | 0 | 52 | 173 | 0 | 0 | 225 | 869 |
| Hourly Total | 0 | 84 | 422 | 215 | 0 | 721 | 0 | 26 | 172 | 226 | 0 | 424 | 0 | 175 | 793 | 73 | 0 | 1041 | 0 | 172 | 641 | 0 | 0 | 813 | 2999 |
| 8:00 AM | 0 | 33 | 111 | 97 | 0 | 241 | 0 | 5 | 72 | 45 | 0 | 122 | 0 | 48 | 169 | 9 | 0 | 226 | 0 | 48 | 179 | 0 | 0 | 227 | 816 |
| 8:15 AM | 0 | 34 | 109 | 76 | 0 | 219 | 0 | 10 | 63 | 59 | 0 | 132 | 0 | 52 | 184 | 12 | 0 | 248 | 0 | 54 | 184 | 0 | 0 | 238 | 837 |
| 8:30 AM | 0 | 18 | 91 | 57 | 0 | 166 | 0 | 10 | 58 | 60 | 0 | 128 | 0 | 37 | 184 | 13 | 0 | 234 | 1 | 43 | 169 | 0 | 0 | 213 | 741 |
| 8:45 AM | 0 | 26 | 94 | 70 | 0 | 190 | 0 | 16 | 88 | 63 | 0 | 167 | 0 | 50 | 161 | 23 | 0 | 234 | 0 | 50 | 201 | 0 | 0 | 251 | 842 |
| Hourly Total | 0 | 111 | 405 | 300 | 0 | 816 | 0 | 41 | 281 | 227 | 0 | 549 | 0 | 187 | 698 | 57 | 0 | 942 | 1 | 195 | 733 | 0 | 0 | 929 | 3236 |
| *** BREAK *** | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| 4:00 PM | 0 | 23 | 74 | 79 | 0 | 176 | 0 | 25 | 135 | 62 | 0 | 222 | 0 | 86 | 219 | 12 | 0 | 317 | 1 | 62 | 233 | 2 | 0 | 298 | 1013 |
| 4:15 PM | 0 | 35 | 78 | 74 | 0 | 187 | 0 | 29 | 107 | 74 | 0 | 210 | 0 | 80 | 228 | 13 | 0 | 321 | 0 | 57 | 233 | 0 | 0 | 290 | 1008 |
| 4:30 PM | 0 | 26 | 76 | 85 | 0 | 187 | 0 | 27 | 127 | 54 | 0 | 208 | 0 | 92 | 230 | 11 | 0 | 333 | 0 | 56 | 279 | 1 | 0 | 336 | 1064 |
| 4:45 PM | 0 | 39 | 68 | 92 | 0 | 199 | 0 | 22 | 121 | 66 | 0 | 209 | 0 | 82 | 228 | 9 | 0 | 319 | 0 | 54 | 252 | 0 | 0 | 306 | 1033 |
| Hourly Total | 0 | 123 | 296 | 330 | 0 | 749 | 0 | 103 | 490 | 256 | 0 | 849 | 0 | 340 | 905 | 45 | 0 | 1290 | 1 | 229 | 997 | 3 | 0 | 1230 | 4118 |
| 5:00 PM | 0 | 28 | 86 | 73 | 0 | 187 | 0 | 22 | 81 | 49 | 0 | 152 | 0 | 81 | 286 | 14 | 0 | 381 | 1 | 60 | 218 | 0 | 0 | 279 | 999 |
| 5:15 PM | 0 | 33 | 81 | 70 | 0 | 184 | 0 | 19 | 115 | 69 | 0 | 203 | 0 | 94 | 247 | 11 | 0 | 352 | 1 | 64 | 250 | 0 | 0 | 315 | 1054 |
| 5:30 PM | 0 | 38 | 61 | 70 | 0 | 169 | 0 | 26 | 101 | 54 | 0 | 181 | 0 | 69 | 218 | 15 | 0 | 302 | 0 | 49 | 228 | 0 | 0 | 277 | 929 |
| 5:45 PM | 0 | 28 | 54 | 68 | 0 | 150 | 0 | 35 | 78 | 46 | 0 | 159 | 1 | 87 | 214 | 12 | 0 | 314 | 0 | 62 | 165 | 0 | 0 | 227 | 850 |
| Hourly Total | 0 | 127 | 282 | 281 | 0 | 690 | 0 | 102 | 375 | 218 | 0 | 695 | 1 | 331 | 965 | 52 | 0 | 1349 | 2 | 235 | 861 | 0 | 0 | 1098 | 3832 |


| Grand Total | 0 | 834 | 2183 | 1855 | 0 | 4872 | 0 | 505 | 2056 | 1383 | 0 | 3944 | 3 | 1759 | 5551 | 374 | 2 | 7687 | 8 | 1336 | 5371 | 3 | 0 | 6718 | 23221 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach \% | 0.0 | 17.1 | 44.8 | 38.1 | - | - | 0.0 | 12.8 | 52.1 | 35.1 | - | - | 0.0 | 22.9 | 72.2 | 4.9 | - | - | 0.1 | 19.9 | 79.9 | 0.0 | - | - | - |
| Total \% | 0.0 | 3.6 | 9.4 | 8.0 | - | 21.0 | 0.0 | 2.2 | 8.9 | 6.0 | - | 17.0 | 0.0 | 7.6 | 23.9 | 1.6 | - | 33.1 | 0.0 | 5.8 | 23.1 | 0.0 | - | 28.9 | - |
| Lights | 0 | 817 | 2137 | 1801 | - | 4755 | 0 | 496 | 2033 | 1315 | - | 3844 | 3 | 1710 | 5351 | 363 | - | 7427 | 8 | 1286 | 5181 | 3 | - | 6478 | 22504 |
| \% Lights | - | 98.0 | 97.9 | 97.1 | - | 97.6 | - | 98.2 | 98.9 | 95.1 | - | 97.5 | 100.0 | 97.2 | 96.4 | 97.1 | - | 96.6 | 100.0 | 96.3 | 96.5 | 100.0 | - | 96.4 | 96.9 |
| Buses | 0 | 3 | 4 | 13 | - | 20 | 0 | 1 | 2 | 3 | - | 6 | 0 | 22 | 23 | 0 | - | 45 | 0 | 6 | 26 | 0 | - | 32 | 103 |
| \% Buses | - | 0.4 | 0.2 | 0.7 | - | 0.4 | - | 0.2 | 0.1 | 0.2 | - | 0.2 | 0.0 | 1.3 | 0.4 | 0.0 | - | 0.6 | 0.0 | 0.4 | 0.5 | 0.0 | - | 0.5 | 0.4 |
| Single-Unit Trucks | 0 | 9 | 15 | 32 | - | 56 | 0 | 6 | 10 | 49 | - | 65 | 0 | 17 | 95 | 10 | - | 122 | 0 | 29 | 96 | 0 | - | 125 | 368 |
| $\begin{gathered} \% \text { Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 1.1 | 0.7 | 1.7 | - | 1.1 | - | 1.2 | 0.5 | 3.5 | - | 1.6 | 0.0 | 1.0 | 1.7 | 2.7 | - | 1.6 | 0.0 | 2.2 | 1.8 | 0.0 | - | 1.9 | 1.6 |
| Articulated Trucks | 0 | 3 | 17 | 9 | - | 29 | 0 | 2 | 7 | 16 | - | 25 | 0 | 8 | 82 | 1 | - | 91 | 0 | 15 | 68 | 0 | - | 83 | 228 |
| \% Articulated Trucks | - | 0.4 | 0.8 | 0.5 | . | 0.6 | . | 0.4 | 0.3 | 1.2 | . | 0.6 | 0.0 | 0.5 | 1.5 | 0.3 | - | 1.2 | 0.0 | 1.1 | 1.3 | 0.0 | - | 1.2 | 1.0 |
| Bicycles on Road | 0 | 2 | 10 | 0 | - | 12 | 0 | 0 | 4 | 0 | - | 4 | 0 | 2 | 0 | 0 | - | 2 | 0 | 0 | 0 | 0 | - | 0 | 18 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \\ \hline \end{gathered}$ | - | 0.2 | 0.5 | 0.0 | - | 0.2 | - | 0.0 | 0.2 | 0.0 | - | 0.1 | 0.0 | 0.1 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | $\checkmark$ | - | - | 2 | - | - | - | - | - | 0 | $\cdot$ | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 100.0 | - | - | - | - | - | - | - | - | 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018
Count Name: Deerfield Road with Milwaukee
(847)518-9990

Avenue
Site Code:
05/08/2021
Page No: 3

Turning Movement Peak Hour Data (12:00 PM)

| Start Time | Deerfield Road Eastbound |  |  |  |  |  | Deerfield Road Westbound |  |  |  |  |  | Milwaukee Avenue Northbound |  |  |  |  |  | Milwaukee Avenue Southbound |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. <br> Total | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \\ & \hline \end{aligned}$ | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App. } \\ & \text { Total } \end{aligned}$ | Int. Total |
| 12:00 PM | 0 | 32 | 97 | 89 | 0 | 218 | 0 | 32 | 75 | 57 | 0 | 164 | 0 | 81 | 219 | 20 | 0 | 320 | 2 | 56 | 200 | 0 | 0 | 258 | 960 |
| 12:15 PM | 0 | 31 | 74 | 71 | 0 | 176 | 0 | 11 | 76 | 37 | 0 | 124 | 0 | 91 | 243 | 12 | 0 | 346 | 0 | 44 | 222 | 0 | 0 | 266 | 912 |
| 12:30 PM | 0 | 43 | 94 | 82 | 0 | 219 | 0 | 23 | 74 | 32 | 0 | 129 | 1 | 67 | 193 | 12 | 0 | 273 | 0 | 57 | 208 | 0 | 0 | 265 | 886 |
| 12:45 PM | 0 | 44 | 68 | 77 | 0 | 189 | 0 | 16 | 64 | 48 | 0 | 128 | 0 | 71 | 252 | 13 | 0 | 336 | 0 | 52 | 242 | 0 | 0 | 294 | 947 |
| Total | 0 | 150 | 333 | 319 | 0 | 802 | 0 | 82 | 289 | 174 | 0 | 545 | 1 | 310 | 907 | 57 | 0 | 1275 | 2 | 209 | 872 | 0 | 0 | 1083 | 3705 |
| Approach \% | 0.0 | 18.7 | 41.5 | 39.8 | - | - | 0.0 | 15.0 | 53.0 | 31.9 | - | - | 0.1 | 24.3 | 71.1 | 4.5 | - | - | 0.2 | 19.3 | 80.5 | 0.0 | - | - | - |
| Total \% | 0.0 | 4.0 | 9.0 | 8.6 | - | 21.6 | 0.0 | 2.2 | 7.8 | 4.7 | - | 14.7 | 0.0 | 8.4 | 24.5 | 1.5 | - | 34.4 | 0.1 | 5.6 | 23.5 | 0.0 | - | 29.2 | - |
| PHF | 0.000 | 0.852 | 0.858 | 0.896 | - | 0.916 | 0.000 | 0.641 | 0.951 | 0.763 | - | 0.831 | 0.250 | 0.852 | 0.900 | 0.713 | - | 0.921 | 0.250 | 0.917 | 0.901 | 0.000 | - | 0.921 | 0.965 |
| Lights | 0 | 150 | 322 | 315 | - | 787 | 0 | 80 | 288 | 164 | - | 532 | 1 | 306 | 887 | 57 | - | 1251 | 2 | 200 | 861 | 0 | - | 1063 | 3633 |
| \% Lights | - | 100.0 | 96.7 | 98.7 | - | 98.1 | - | 97.6 | 99.7 | 94.3 | - | 97.6 | 100.0 | 98.7 | 97.8 | 100.0 | - | 98.1 | 100.0 | 95.7 | 98.7 | - | - | 98.2 | 98.1 |
| Buses | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 2 | 0 | - | 2 | 0 | 0 | 0 | 0 | - | 0 | 3 |
| \% Buses | - | 0.0 | 0.0 | 0.3 | - | 0.1 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.2 | 0.0 | - | 0.2 | 0.0 | 0.0 | 0.0 | - | - | 0.0 | 0.1 |
| Single-Unit Trucks | 0 | 0 | 3 | 2 | - | 5 | 0 | 2 | 1 | 10 | - | 13 | 0 | 3 | 13 | 0 | $\checkmark$ | 16 | 0 | 7 | 9 | 0 | $\checkmark$ | 16 | 50 |
| \% Single-Unit Trucks | - | 0.0 | 0.9 | 0.6 | - | 0.6 | - | 2.4 | 0.3 | 5.7 | - | 2.4 | 0.0 | 1.0 | 1.4 | 0.0 | - | 1.3 | 0.0 | 3.3 | 1.0 | . | - | 1.5 | 1.3 |
| Articulated Trucks | 0 | 0 | 0 | 1 | - | 1 | 0 | 0 | 0 | 0 | - | 0 | 0 | 1 | 5 | 0 | - | 6 | 0 | 2 | 2 | 0 | - | 4 | 11 |
| \% Articulated Trucks | - | 0.0 | 0.0 | 0.3 | - | 0.1 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.3 | 0.6 | 0.0 | - | 0.5 | 0.0 | 1.0 | 0.2 | - | - | 0.4 | 0.3 |
| Bicycles on Road | 0 | 0 | 8 | 0 | - | 8 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 8 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \end{gathered}$ | . | 0.0 | 2.4 | 0.0 | - | 1.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.0 | 0.0 | 0.0 | . | - | 0.0 | 0.2 |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 9575 W. Higgins Rd., Suite 400

Turning Movement Peak Hour Data (7:30 AM)

| Start Time | Deerfield Road Eastbound |  |  |  |  |  | Deerfield Road Westbound |  |  |  |  |  | Milwaukee Avenue Northbound |  |  |  |  |  | Milwaukee Avenue Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. |  |
| 7:30 AM | 0 | 24 | 102 | 64 | 0 | 190 | 0 | 13 | 45 | 51 | 0 | 109 | 0 | 41 | 222 | 15 | 0 | 278 | 0 | 49 | 170 | 0 | 0 | 219 | 796 |
| 7:45 AM | 0 | 27 | 120 | 65 | 0 | 212 | 0 | 5 | 45 | 70 | 0 | 120 | 0 | 60 | 233 | 19 | 0 | 312 | 0 | 52 | 173 | 0 | 0 | 225 | 869 |
| 8:00 AM | 0 | 33 | 111 | 97 | 0 | 241 | 0 | 5 | 72 | 45 | 0 | 122 | 0 | 48 | 169 | 9 | 0 | 226 | 0 | 48 | 179 | 0 | 0 | 227 | 816 |
| 8:15 AM | 0 | 34 | 109 | 76 | 0 | 219 | 0 | 10 | 63 | 59 | 0 | 132 | 0 | 52 | 184 | 12 | 0 | 248 | 0 | 54 | 184 | 0 | 0 | 238 | 837 |
| Total | 0 | 118 | 442 | 302 | 0 | 862 | 0 | 33 | 225 | 225 | 0 | 483 | 0 | 201 | 808 | 55 | 0 | 1064 | 0 | 203 | 706 | 0 | 0 | 909 | 3318 |
| Approach \% | 0.0 | 13.7 | 51.3 | 35.0 | - | - | 0.0 | 6.8 | 46.6 | 46.6 | - | - | 0.0 | 18.9 | 75.9 | 5.2 | - | - | 0.0 | 22.3 | 77.7 | 0.0 | - | - | - |
| Total \% | 0.0 | 3.6 | 13.3 | 9.1 | - | 26.0 | 0.0 | 1.0 | 6.8 | 6.8 | - | 14.6 | 0.0 | 6.1 | 24.4 | 1.7 | - | 32.1 | 0.0 | 6.1 | 21.3 | 0.0 | - | 27.4 | - |
| PHF | 0.000 | 0.868 | 0.921 | 0.778 | - | 0.894 | 0.000 | 0.635 | 0.781 | 0.804 | - | 0.915 | 0.000 | 0.838 | 0.867 | 0.724 | - | 0.853 | 0.000 | 0.940 | 0.959 | 0.000 | - | 0.955 | 0.955 |
| Lights | 0 | 114 | 424 | 288 | - | 826 | 0 | 31 | 224 | 214 | - | 469 | 0 | 187 | 751 | 51 | - | 989 | 0 | 191 | 656 | 0 | - | 847 | 3131 |
| \% Lights | - | 96.6 | 95.9 | 95.4 | - | 95.8 | - | 93.9 | 99.6 | 95.1 | - | 97.1 | - | 93.0 | 92.9 | 92.7 | - | 93.0 | - | 94.1 | 92.9 | - | - | 93.2 | 94.4 |
| Buses | 0 | 0 | 3 | 1 | - | 4 | 0 | 0 | 0 | 0 | - | 0 | 0 | 9 | 6 | 0 | - | 15 | 0 | 1 | 10 | 0 | - | 11 | 30 |
| \% Buses | - | 0.0 | 0.7 | 0.3 | - | 0.5 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 4.5 | 0.7 | 0.0 | - | 1.4 | - | 0.5 | 1.4 | - | - | 1.2 | 0.9 |
| Single-Unit Trucks | 0 | 3 | 4 | 12 | - | 19 | 0 | 2 | 0 | 8 | - | 10 | 0 | 3 | 28 | 3 | - | 34 | 0 | 8 | 26 | 0 | $\checkmark$ | 34 | 97 |
| $\begin{gathered} \text { \% Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 2.5 | 0.9 | 4.0 | - | 2.2 | - | 6.1 | 0.0 | 3.6 | - | 2.1 | - | 1.5 | 3.5 | 5.5 | - | 3.2 | - | 3.9 | 3.7 | - | - | 3.7 | 2.9 |
| Articulated Trucks | 0 | 1 | 11 | 1 | - | 13 | 0 | 0 | 1 | 3 | - | 4 | 0 | 2 | 23 | 1 | $\checkmark$ | 26 | 0 | 3 | 14 | 0 | - | 17 | 60 |
| \% Articulated Trucks | - | 0.8 | 2.5 | 0.3 | - | 1.5 | . | 0.0 | 0.4 | 1.3 | - | 0.8 | . | 1.0 | 2.8 | 1.8 | - | 2.4 | . | 1.5 | 2.0 | . | - | 1.9 | 1.8 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | $\checkmark$ | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | $\cdots$ | 0 | 0 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \\ \hline \end{gathered}$ | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.0 | - | - | 0.0 | 0.0 |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 9575 W. Higgins Rd., Suite 400

Turning Movement Peak Hour Data (4:30 PM)

| Start Time | Deerfield Road Eastbound |  |  |  |  |  | Deerfield Road Westbound |  |  |  |  |  | Milwaukee Avenue Northbound |  |  |  |  |  | Milwaukee Avenue Southbound |  |  |  |  |  | Int. Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | U-Turn | Left | Thru | Right | Peds | $\begin{aligned} & \text { App. } \\ & \hline \text { Total } \end{aligned}$ | U-Turn | Left | Thru | Right | Peds | App. | U-Turn | Left | Thru | Right | Peds | App. Total | U-Turn | Left | Thru | Right | Peds | App. Total |  |
| 4:30 PM | 0 | 26 | 76 | 85 | 0 | 187 | 0 | 27 | 127 | 54 | 0 | 208 | 0 | 92 | 230 | 11 | 0 | 333 | 0 | 56 | 279 | 1 | 0 | 336 | 1064 |
| 4:45 PM | 0 | 39 | 68 | 92 | 0 | 199 | 0 | 22 | 121 | 66 | 0 | 209 | 0 | 82 | 228 | 9 | 0 | 319 | 0 | 54 | 252 | 0 | 0 | 306 | 1033 |
| 5:00 PM | 0 | 28 | 86 | 73 | 0 | 187 | 0 | 22 | 81 | 49 | 0 | 152 | 0 | 81 | 286 | 14 | 0 | 381 | 1 | 60 | 218 | 0 | 0 | 279 | 999 |
| 5:15 PM | 0 | 33 | 81 | 70 | 0 | 184 | 0 | 19 | 115 | 69 | 0 | 203 | 0 | 94 | 247 | 11 | 0 | 352 | 1 | 64 | 250 | 0 | 0 | 315 | 1054 |
| Total | 0 | 126 | 311 | 320 | 0 | 757 | 0 | 90 | 444 | 238 | 0 | 772 | 0 | 349 | 991 | 45 | 0 | 1385 | 2 | 234 | 999 | 1 | 0 | 1236 | 4150 |
| Approach \% | 0.0 | 16.6 | 41.1 | 42.3 | - | - | 0.0 | 11.7 | 57.5 | 30.8 | - | - | 0.0 | 25.2 | 71.6 | 3.2 | - | - | 0.2 | 18.9 | 80.8 | 0.1 | - | - | - |
| Total \% | 0.0 | 3.0 | 7.5 | 7.7 | - | 18.2 | 0.0 | 2.2 | 10.7 | 5.7 | - | 18.6 | 0.0 | 8.4 | 23.9 | 1.1 | - | 33.4 | 0.0 | 5.6 | 24.1 | 0.0 | - | 29.8 | - |
| PHF | 0.000 | 0.808 | 0.904 | 0.870 | - | 0.951 | 0.000 | 0.833 | 0.874 | 0.862 | - | 0.923 | 0.000 | 0.928 | 0.866 | 0.804 | - | 0.909 | 0.500 | 0.914 | 0.895 | 0.250 | - | 0.920 | 0.975 |
| Lights | 0 | 123 | 309 | 309 | - | 741 | 0 | 88 | 436 | 225 | - | 749 | 0 | 340 | 960 | 44 | - | 1344 | 2 | 230 | 969 | 1 | - | 1202 | 4036 |
| \% Lights | - | 97.6 | 99.4 | 96.6 | - | 97.9 | - | 97.8 | 98.2 | 94.5 | - | 97.0 | - | 97.4 | 96.9 | 97.8 | - | 97.0 | 100.0 | 98.3 | 97.0 | 100.0 | - | 97.2 | 97.3 |
| Buses | 0 | 2 | 1 | 4 | - | 7 | 0 | 1 | 1 | 1 | - | 3 | 0 | 1 | 1 | 0 | - | 2 | 0 | 1 | 4 | 0 | - | 5 | 17 |
| \% Buses | - | 1.6 | 0.3 | 1.3 | - | 0.9 | - | 1.1 | 0.2 | 0.4 | - | 0.4 | - | 0.3 | 0.1 | 0.0 | - | 0.1 | 0.0 | 0.4 | 0.4 | 0.0 | - | 0.4 | 0.4 |
| Single-Unit Trucks | 0 | 1 | 0 | 4 | - | 5 | 0 | 0 | 3 | 9 | - | 12 | 0 | 2 | 8 | 1 | - | 11 | 0 | 2 | 12 | 0 | $\checkmark$ | 14 | 42 |
| $\begin{gathered} \text { \% Single-Unit } \\ \text { Trucks } \\ \hline \end{gathered}$ | - | 0.8 | 0.0 | 1.3 | - | 0.7 | - | 0.0 | 0.7 | 3.8 | - | 1.6 | - | 0.6 | 0.8 | 2.2 | - | 0.8 | 0.0 | 0.9 | 1.2 | 0.0 | - | 1.1 | 1.0 |
| Articulated Trucks | 0 | 0 | 1 | 3 | - | 4 | 0 | 1 | 3 | 3 | - | 7 | 0 | 4 | 22 | 0 | $\checkmark$ | 26 | 0 | 1 | 14 | 0 | - | 15 | 52 |
| \% Articulated Trucks | - | 0.0 | 0.3 | 0.9 | - | 0.5 | - | 1.1 | 0.7 | 1.3 | - | 0.9 | . | 1.1 | 2.2 | 0.0 | - | 1.9 | 0.0 | 0.4 | 1.4 | 0.0 | - | 1.2 | 1.3 |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 1 | 0 | - | 1 | 0 | 2 | 0 | 0 | - | 2 | 0 | 0 | 0 | 0 | - | 0 | 3 |
| $\begin{gathered} \text { \% Bicycles on } \\ \text { Road } \\ \hline \end{gathered}$ | - | 0.0 | 0.0 | 0.0 | - | 0.0 | - | 0.0 | 0.2 | 0.0 | - | 0.1 | - | 0.6 | 0.0 | 0.0 | - | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: Deerfield Road with West Drive Site Code:
Start Date: 05/08/2021
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| Approach \% | 0.1 | 1.2 | 98.8 | - | - | 0.0 | 97.8 | 2.2 | - | - | 0.0 | 36.8 | 63.2 | - | - | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Total \% | 0.0 | 0.5 | 46.3 | - | 46.8 | 0.0 | 49.2 | 1.1 | - | 50.3 | 0.0 | 1.1 | 1.8 | - | 2.9 | - |
| Lights | 3 | 39 | 3399 | - | 3441 | 0 | 3606 | 82 | - | 3688 | 0 | 81 | 138 | - | 219 | 7348 |
| \% Lights | 100.0 | 95.1 | 97.2 | - | 97.2 | - | 97.0 | 100.0 | - | 97.1 | - | 100.0 | 99.3 | - | 99.5 | 97.2 |
| Buses | 0 | 0 | 6 | - | 6 | 0 | 7 | 0 | - | 7 | 0 | 0 | 0 | - | 0 | 13 |
| \% Buses | 0.0 | 0.0 | 0.2 | - | 0.2 | - | 0.2 | 0.0 | - | 0.2 | - | 0.0 | 0.0 | - | 0.0 | 0.2 |
| Single-Unit Trucks | 0 | 2 | 52 | - | 54 | 0 | 69 | 0 | - | 69 | 0 | 0 | 1 | - | 1 | 124 |
| \% Single-Unit Trucks | 0.0 | 4.9 | 1.5 | - | 1.5 | - | 1.9 | 0.0 | - | 1.8 | - | 0.0 | 0.7 | - | 0.5 | 1.6 |
| Articulated Trucks | 0 | 0 | 32 | - | 32 | 0 | 33 | 0 | - | 33 | 0 | 0 | 0 | - | 0 | 65 |
| \% Articulated Trucks | 0.0 | 0.0 | 0.9 | - | 0.9 | - | 0.9 | 0.0 | - | 0.9 | - | 0.0 | 0.0 | - | 0.0 | 0.9 |
| Bicycles on Road | 0 | 0 | 8 | - | 8 | 0 | 2 | 0 | - | 2 | 0 | 0 | 0 |  | 0 | 10 |
| \% Bicycles on Road | 0.0 | 0.0 | 0.2 | - | 0.2 | - | 0.1 | 0.0 | - | 0.1 | - | 0.0 | 0.0 | - | 0.0 | 0.1 |
| Pedestrians | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - |
| \% Pedestrians | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | 9575 W. Higgins Rd., Suite 400

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Count Name: Deerfield Road with West Drive Site Code:
Star Date: 05/08/2021
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Turning Movement Peak Hour Data (12:00 PM)
 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018 (847)518-9990

Count Name: Deerfield Road with West Drive Site Code:

08/2021
Page No: 4

Turning Movement Peak Hour Data (12:00 AM)
 9575 W. Higgins Rd., Suite 400

Rosemont, Illinois, United States 60018
Count Name: Deerfield Road with West Drive Site Code:
(847)518-9990

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Turning Movement Peak Hour Data (4:30 PM)



## Study Name Deerfield Road with East Access Drives Start Date <br> Start Date Saturday, May 08, 2021 11:30 AM End Date Tuesday, May 11, 2021 6:00 PM

Report Summary


TURNS/TEAPAC[Ver 3.61.12] - 15-Minute Counts: All Vehicles - by Mvmt

| Begin Time | Intersection \# 5 deerfield/chicory |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | N-Approach |  |  | E-Approach |  |  | S-Approach |  |  | W-Approach |  |  | Int Total |
|  | RT | TH | LT | RT | TH | LT | RT | TH | LT | RT | TH | LT |  |
| 630 | 1 | 0 | 3 | 0 | 66 | 0 | 0 | 0 | 0 | 0 | 108 | 0 | 178 |
| 645 | 1 | 0 | 0 | 2 | 104 | 0 | 0 | 0 | 0 | 0 | 156 | 1 | 264 |
| 700 | 1 | 0 | 2 | 0 | 102 | 0 | 0 | 0 | 0 | 0 | 137 | 1 | 243 |
| 715 | 1 | 0 | 2 | 0 | 110 | 0 | 0 | 0 | 0 | 0 | 171 | 0 | 284 |
| 730 | 0 | 0 | 4 | 1 | 136 | 0 | 0 | 0 | 0 | 0 | 188 | 0 | 329 |
| 745 | 0 | 0 | 3 | 0 | 122 | 0 | 0 | 0 | 0 | 0 | 157 | 0 | 282 |
| 800 | 0 | 0 | 3 | 1 | 150 | 0 | 0 | 0 | 0 | 0 | 201 | 1 | 356 |
| 815 | 2 | 0 | 4 | 3 | 140 | 0 | 0 | 0 | 0 | 0 | 165 | 0 | 314 |
| 830 | 2 | 0 | 2 | 0 | 152 | 0 | 0 | 0 | 0 | 0 | 200 | 1 | 357 |
| 845 | 1 | 0 | 2 | 0 | 136 | 0 | 0 | 0 | 0 | 0 | 189 | 1 | 329 |
| 1600 | 0 | 0 | 0 | 3 | 182 | 0 | 0 | 0 | 0 | 0 | 145 | 0 | 330 |
| 1615 | 0 | 0 | 2 | 2 | 192 | 0 | 0 | 0 | 0 | 0 | 145 | 0 | 341 |
| 1630 | 0 | 0 | 1 | 3 | 208 | 0 | 0 | 0 | 0 | 0 | 147 | 1 | 360 |
| 1645 | 0 | 0 | 0 | 0 | 215 | 0 | 0 | 0 | 0 | 0 | 135 | 0 | 350 |
| 1700 | 1 | 0 | 3 | 1 | 195 | 0 | 0 | 0 | 0 | 0 | 172 | 1 | 373 |
| 1715 | 1 | 0 | 1 | 3 | 200 | 0 | 0 | 0 | 0 | 0 | 156 | 2 | 363 |
| 1730 | 0 | 0 | 1 | 1 | 230 | 0 | 0 | 0 | 0 | 0 | 150 | 0 | 382 |
| 1745 | 1 | 0 | 0 | 4 | 177 | 0 | 0 | 0 | 0 | 0 | 128 | 1 | 311 |
| 1800 | 1 | 0 | 0 | 4 | 145 | 0 | 0 | 0 | 0 | 0 | 117 | 3 | 270 |
| 1815 | 3 | 0 | 3 | 3 | 143 | 0 | 0 | 0 | 0 | 0 | 135 | 1 | 288 |
| Total | 16 | 0 | 36 | 31 | 3105 | 0 | 0 | 0 | 0 | 0 | 3102 | 14 | 6304 |

Milwaukee Avenue with Deerfield Road IDS




## Preliminary Site Plan



## Level of Service Criteria



Capacity Analysis Summary Sheets Year 2021 Weekday Morning Peak Hour Conditions

|  | 4 | $\rightarrow$ |  | 4 |  |  |  | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 44 | 7 | ${ }^{7}$ | 車 $\hat{p}$ |  | 7 | 中 $\hat{\beta}$ |  | ${ }^{7} 1$ | 中4 | F |
| Traffic Volume（vph） | 54 | 513 | 475 | 77 | 266 | 496 | 235 | 1128 | 132 | 436 | 1049 | 34 |
| Future Volume（vph） | 54 | 513 | 475 | 77 | 266 | 496 | 235 | 1128 | 132 | 436 | 1049 | 34 |
| Ideal Flow（vphpl） | 1900 | 2000 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 2000 | 1900 |
| Lane Width（ft） | 12 | 12 | 12 | 12 | 12 | 12 | 11 | 12 | 12 | 11 | 11 | 11 |
| Grade（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Storage Length（ft） | 190 |  | 275 | 300 |  | 0 | 460 |  | 0 | 500 |  | 640 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 2 |  | 0 | 2 |  | 1 |
| Taper Length（ft） | 190 |  |  | 125 |  |  | 300 |  |  | 300 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.95 | 0.97 | 0.95 | 0.95 | 0.97 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  | 0.850 |  | 0.902 |  |  | 0.984 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1752 | 3654 | 1538 | 1703 | 3143 | 0 | 3164 | 3320 | 0 | 3193 | 3433 | 1561 |
| Flt Permitted | 0.159 |  |  | 0.221 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（perm） | 293 | 3654 | 1538 | 396 | 3143 | 0 | 3164 | 3320 | 0 | 3193 | 3433 | 1561 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 118 |  | 338 |  |  | 11 |  |  |  | 65 |
| Link Speed（mph） |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance（ft） |  | 873 |  |  | 312 |  |  | 454 |  |  | 1660 |  |
| Travel Time（s） |  | 14.9 |  |  | 5.3 |  |  | 7.7 |  |  | 28.3 |  |
| Confl．Peds．（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ |
| Heavy Vehicles（\％） | 3\％ | 4\％ | 5\％ | 6\％ | 1\％ | 5\％ | 7\％ | 7\％ | 7\％ | 6\％ | 7\％ | 0\％ |
| Bus Blockages（\＃／hr） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid－Block Traffic（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 56 | 534 | 495 | 80 | 794 | 0 | 245 | 1313 | 0 | 454 | 1093 | 35 |
| Turn Type | pm＋pt | NA | pm＋ov | pm＋pt | NA |  | Prot | NA |  | Prot | NA | pm＋ov |
| Protected Phases | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Permitted Phases | 4 |  | 4 | 8 |  |  |  |  |  |  |  | 6 |
| Detector Phase | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 8.0 | 4.0 | 3.0 | 8.0 |  | 4.0 | 15.0 |  | 4.0 | 15.0 | 3.0 |
| Minimum Split（s） | 6.5 | 14.0 | 8.5 | 6.5 | 14.0 |  | 8.5 | 21.0 |  | 8.5 | 43.0 | 6.5 |
| Total Split（s） | 14.0 | 31.0 | 21.0 | 14.0 | 31.0 |  | 21.0 | 52.0 |  | 28.0 | 59.0 | 14.0 |
| Total Split（\％） | 11．2\％ | 24．8\％ | 16．8\％ | 11．2\％ | 24．8\％ |  | 16．8\％ | 41．6\％ |  | 22．4\％ | 47．2\％ | 11．2\％ |
| Yellow Time（s） | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 |  | 3.5 | 4.5 |  | 3.5 | 4.5 | 3.5 |
| All－Red Time（s） | 0.0 | 1.5 | 1.0 | 0.0 | 1.5 |  | 1.0 | 1.5 |  | 1.0 | 1.5 | 0.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.5 | 6.0 | 4.5 | 3.5 | 6.0 |  | 4.5 | 6.0 |  | 4.5 | 6.0 | 3.5 |
| Lead／Lag | Lead | Lag | Lead | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lead |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None |  | None | C－Min |  | None | C－Min | None |
| Act Effct Green（s） | 34.7 | 25.1 | 45.7 | 36.1 | 25.8 |  | 14.5 | 51.3 |  | 21.5 | 58.3 | 72.5 |
| Actuated g／C Ratio | 0.28 | 0.20 | 0.37 | 0.29 | 0.21 |  | 0.12 | 0.41 |  | 0.17 | 0.47 | 0.58 |


|  | $\stackrel{ }{*}$ |  |  | $\downarrow$ |  |  | - | $\dagger$ |  |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.32 | 0.73 | 0.78 | 0.38 | 0.87 |  | 0.67 | 0.96 |  | 0.83 | 0.68 | 0.04 |
| Control Delay | 34.2 | 53.3 | 35.6 | 35.5 | 38.0 |  | 61.9 | 53.4 |  | 63.1 | 30.3 | 0.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.2 | 53.3 | 35.6 | 35.5 | 38.0 |  | 61.9 | 53.4 |  | 63.1 | 30.3 | 0.8 |
| LOS | C | D | D | D | D |  | E | D |  | E | C | A |
| Approach Delay |  | 44.2 |  |  | 37.8 |  |  | 54.8 |  |  | 39.1 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | D |  |
| Queue Length 50th (ft) | 31 | 212 | 268 | 45 | 194 |  | 97 | $\sim 607$ |  | 182 | 383 | 0 |
| Queue Length 95th (tt) | 63 | 278 | 412 | 84 | \#310 |  | 142 | \#757 |  | 241 | 472 | 5 |
| Internal Link Dist (tt) |  | 793 |  |  | 232 |  |  | 374 |  |  | 1580 |  |
| Turn Bay Length (tt) | 190 |  | 275 | 300 |  |  | 460 |  |  | 500 |  | 640 |
| Base Capacity (vph) | 206 | 749 | 658 | 226 | 929 |  | 417 | 1368 |  | 600 | 1600 | 959 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.27 | 0.71 | 0.75 | 0.35 | 0.85 |  | 0.59 | 0.96 |  | 0.76 | 0.68 | 0.04 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 125 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 125 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 72 (58\%), Referenced to phase 2:NBT and 6:SBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 0.96 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 44.7 |  |  |  |  | Intersection LOS: D |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 91.6\% |  |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Milwaukee Avenue \& Deerfield Road


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 880 | 0 | - | 0 | 1444 | 440 |
| Stage 1 | - | - | - |  | 876 | - |
| Stage 2 | - | - | - | - | 568 | - |
| Critical Hdwy | 4.76 | - | - | - | 6.8 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.8 | - |
| Critical Hdwy Stg 2 | - | - | - |  | 5.8 | - |
| Follow-up Hdwy | 2.53 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 596 | - | - | - | 125 | 570 |
| Stage 1 | - |  | - |  | 373 | - |
| Stage 2 | - | - | - |  | 536 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 596 | - | - | - | 123 | 570 |
| Mov Cap-2 Maneuver | - | - | - |  | 123 | - |
| Stage 1 | - |  | - |  | 368 | - |
| Stage 2 | - | - | - |  | 536 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.1 |  | 0 |  | 23.2 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR | SBLn1 |
| Capacity (veh/h) |  | 596 | - | - | - | 202 |
| HCM Lane V/C Ratio |  | 0.005 | - | - |  | 0.021 |
| HCM Control Delay (s) |  | 11.1 | 0.1 |  |  | 23.2 |
| HCM Lane LOS |  | B | A | - | - | C |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 0.1 |






| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



## Capacity Analysis Summary Sheets <br> Year 2021 Weekday Evening Peak Hour Conditions

|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | 4 |  | （ | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 44 | 7 | ${ }^{7}$ | 中 $\%$ |  | ${ }^{7} 1$ | 中 $\%$ |  | ＊ | 44 | 「 |
| Traffic Volume（vph） | 100 | 280 | 312 | 79 | 733 | 303 | 374 | 1313 | 38 | 387 | 1345 | 61 |
| Future Volume（vph） | 100 | 280 | 312 | 79 | 733 | 303 | 374 | 1313 | 38 | 387 | 1345 | 61 |
| Ideal Flow（vphpl） | 1900 | 2000 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 2000 | 1900 |
| Lane Width（ft） | 12 | 12 | 12 | 12 | 12 | 12 | 11 | 12 | 12 | 11 | 11 | 11 |
| Grade（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Storage Length（ft） | 190 |  | 275 | 300 |  | 0 | 460 |  | 0 | 500 |  | 640 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 2 |  | 0 | 2 |  | 1 |
| Taper Length（ft） | 190 |  |  | 125 |  |  | 300 |  |  | 300 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.95 | 0.97 | 0.95 | 0.95 | 0.97 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  | 0.850 |  | 0.956 |  |  | 0.996 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 3762 | 1568 | 1770 | 3355 | 0 | 3286 | 3492 | 0 | 3319 | 3566 | 1561 |
| Flt Permitted | 0.119 |  |  | 0.541 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（perm） | 222 | 3762 | 1568 | 1008 | 3355 | 0 | 3286 | 3492 | 0 | 3319 | 3566 | 1561 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 130 |  | 46 |  |  | 3 |  |  |  | 63 |
| Link Speed（mph） |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance（ft） |  | 873 |  |  | 312 |  |  | 454 |  |  | 1660 |  |
| Travel Time（s） |  | 14.9 |  |  | 5.3 |  |  | 7.7 |  |  | 28.3 |  |
| Confl．Peds．（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ |
| Heavy Vehicles（\％） | 2\％ | 1\％ | 3\％ | 2\％ | 2\％ | 5\％ | 3\％ | 3\％ | 2\％ | 2\％ | 3\％ | 0\％ |
| Bus Blockages（\＃／hr） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid－Block Traffic（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 102 | 286 | 318 | 81 | 1057 | 0 | 382 | 1379 | 0 | 395 | 1372 | 62 |
| Turn Type | pm＋pt | NA | pm＋ov | pm＋pt | NA |  | Prot | NA |  | Prot | NA | pm＋ov |
| Protected Phases | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Permitted Phases | 4 |  | 4 | 8 |  |  |  |  |  |  |  | 6 |
| Detector Phase | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 8.0 | 4.0 | 3.0 | 8.0 |  | 4.0 | 15.0 |  | 4.0 | 15.0 | 3.0 |
| Minimum Split（s） | 6.5 | 14.0 | 8.5 | 6.5 | 14.0 |  | 8.5 | 21.0 |  | 8.5 | 43.0 | 6.5 |
| Total Split（s） | 14.0 | 38.0 | 24.0 | 14.0 | 38.0 |  | 24.0 | 56.0 |  | 22.0 | 54.0 | 14.0 |
| Total Split（\％） | 10．8\％ | 29．2\％ | 18．5\％ | 10．8\％ | 29．2\％ |  | 18．5\％ | 43．1\％ |  | 16．9\％ | 41．5\％ | 10．8\％ |
| Yellow Time（s） | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 |  | 3.5 | 4.5 |  | 3.5 | 4.5 | 3.5 |
| All－Red Time（s） | 0.0 | 1.5 | 1.0 | 0.0 | 1.5 |  | 1.0 | 1.5 |  | 1.0 | 1.5 | 0.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.5 | 6.0 | 4.5 | 3.5 | 6.0 |  | 4.5 | 6.0 |  | 4.5 | 6.0 | 3.5 |
| Lead／Lag | Lead | Lag | Lead | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lead |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None |  | None | C－Min |  | None | C－Min | None |
| Act Effct Green（s） | 45.8 | 33.5 | 58.0 | 44.2 | 32.7 |  | 18.5 | 50.2 |  | 17.3 | 49.0 | 64.8 |
| Actuated g／C Ratio | 0.35 | 0.26 | 0.45 | 0.34 | 0.25 |  | 0.14 | 0.39 |  | 0.13 | 0.38 | 0.50 |


|  |  |  |  |  |  |  | - | $\uparrow$ |  |  | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.53 | 0.29 | 0.41 | 0.21 | 1.20 |  | 0.82 | 1.02 |  | 0.90 | 1.02 | 0.08 |
| Control Delay | 37.4 | 40.1 | 15.7 | 28.4 | 142.6 |  | 69.0 | 69.7 |  | 78.8 | 69.9 | 4.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay | 37.4 | 40.1 | 15.7 | 28.4 | 142.6 |  | 69.0 | 69.7 |  | 78.8 | 69.9 | 4.2 |
| LOS | D | D | B | C | F |  | E | E |  | E | E | A |
| Approach Delay |  | 28.7 |  |  | 134.5 |  |  | 69.5 |  |  | 69.6 |  |
| Approach LOS |  | C |  |  | F |  |  | E |  |  | E |  |
| Queue Length 50th ( t ) | 57 | 102 | 100 | 45 | $\sim 563$ |  | 161 | $\sim 650$ |  | 171 | $\sim 657$ | 0 |
| Queue Length 95th (t) | 99 | 145 | 180 | 82 | \#701 |  | \#220 | \#792 |  | \#258 | \#797 | 23 |
| Internal Link Dist (t) |  | 793 |  |  | 232 |  |  | 374 |  |  | 1580 |  |
| Turn Bay Length (t) | 190 |  | 275 | 300 |  |  | 460 |  |  | 500 |  | 640 |
| Base Capacity (vph) | 203 | 970 | 783 | 416 | 878 |  | 492 | 1349 |  | 446 | 1345 | 818 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.50 | 0.29 | 0.41 | 0.19 | 1.20 |  | 0.78 | 1.02 |  | 0.89 | 1.02 | 0.08 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 33 (25\%), Referenced to phase 2:NBT and 6:SBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.20 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 77.9 |  |  |  |  | Intersection LOS: E |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 101.1\% |  |  |  |  | ICU Level of Service G |  |  |  |  |  |  |  |
|  |  |  |  |  | Analysis Period (min) 15 |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Milwaukee Avenue \& Deerfield Road


| Intersection |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.5 |  |  |  |  |  |
| Movement E | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | * 4 | 中 ${ }^{\text {a }}$ |  | M |  |
| Traffic Vol, veh/h |  | 703 | 1094 | 11 | 13 | 21 |
| Future Vol, veh/h | 2 | 703 | 1094 | 11 | 13 | 21 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
|  | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 1 | 3 | 0 | 0 | 0 |
| Mvmt Flow | 2 | 740 | 1152 | 12 | 14 | 22 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 1164 | 0 | - | 0 | 1532 | 582 |
| Stage 1 | - | - | - | -1158 | - |  |
| Stage 2 | - | - | - | - | 374 | - |
| Critical Hdwy | 4.1 | - | - | - | 6.8 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.8 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.8 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 607 | - | - | - | 110 | 461 |
| $\quad$ Stage 1 | - | - | - | - | 265 | - |
| Stage 2 | - | - | - | - | 672 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 607 | - | - | - | 109 | 461 |
| Mov Cap-2 Maneuver | - | - | - | - | 109 | - |
| Stage 1 | - | - | - | - | 263 | - |
| Stage 2 | - | - | - | - | 672 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 26.1 |
| HCM LOS |  |  | D |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 607 | - | - | - | 206 |
| HCM Lane V/C Ratio | 0.003 | - | - | -0.174 |  |
| HCM Control Delay (s) | 11 | 0 | - | -26.1 |  |
| HCM Lane LOS | B | A | - | - | D |
| HCM 95th \%tile Q(veh) | 0 | - | - | - | 0.6 |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.7 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | $\uparrow$ |  |  | -1 | Mr |  |
| Traffic Vol, veh/h | 713 | 7 | 2 | 1088 | 17 | 6 |
| Future Vol, veh/h | 713 | 7 | 2 | 1088 | 17 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 2 | 0 | 0 | 3 | 0 | 0 |
| Mvmt Flow | 767 | 8 | 2 | 1170 | 18 | 6 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1338 | 0 | - | 0 | 2214 | 1331 |
| Stage 1 |  |  |  |  | 1331 |  |
| Stage 2 | - |  |  |  | 883 |  |
| Critical Hdwy | 4.1 | - | - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 |  |
| Critical Hdwy Stg 2 |  | - |  | - | 5.4 |  |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 522 | - | - | - | 49 | 191 |
| Stage 1 | - | - | - |  | 249 |  |
| Stage 2 | - | - | - | - | 408 |  |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 522 | - | - |  | 48 | 191 |
| Mov Cap-2 Maneuver |  | - | - | - | 48 |  |
| Stage 1 |  | - | - |  | 244 |  |
| Stage 2 | - | - | - |  | 408 |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.1 | 0 | 55.6 |
| HCM LOS |  | F |  |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 522 | - | - | -82 |
| HCM Lane V/C Ratio | 0.012 | - | - | -0.134 |
| HCM Control Delay (s) | 12 | 0 | - | -55.6 |
| HCM Lane LOS | B | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | - | - |
| (ven |  |  |  |  |

Capacity Analysis Summary Sheets No-Build Weekday Morning Peak Hour Conditions

|  | 4 | $\rightarrow$ |  | 4 |  |  |  | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 44 | 7 | ${ }^{7}$ | 㻢 |  | 7 | 中 $\hat{p}$ |  | ${ }^{7} 1$ | 中4 | F |
| Traffic Volume（vph） | 59 | 569 | 518 | 109 | 287 | 541 | 268 | 1246 | 144 | 509 | 1127 | 37 |
| Future Volume（vph） | 59 | 569 | 518 | 109 | 287 | 541 | 268 | 1246 | 144 | 509 | 1127 | 37 |
| Ideal Flow（vphpl） | 1900 | 2000 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 2000 | 1900 |
| Lane Width（ft） | 12 | 12 | 12 | 12 | 12 | 12 | 11 | 12 | 12 | 11 | 11 | 11 |
| Grade（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Storage Length（ft） | 190 |  | 275 | 300 |  | 0 | 460 |  | 0 | 500 |  | 640 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 2 |  | 0 | 2 |  | 1 |
| Taper Length（ft） | 190 |  |  | 125 |  |  | 300 |  |  | 300 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.95 | 0.97 | 0.95 | 0.95 | 0.97 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  | 0.850 |  | 0.902 |  |  | 0.984 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1752 | 3654 | 1538 | 1703 | 3143 | 0 | 3164 | 3320 | 0 | 3193 | 3433 | 1561 |
| Flt Permitted | 0.157 |  |  | 0.161 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（perm） | 290 | 3654 | 1538 | 289 | 3143 | 0 | 3164 | 3320 | 0 | 3193 | 3433 | 1561 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 96 |  | 344 |  |  | 11 |  |  |  | 65 |
| Link Speed（mph） |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance（ft） |  | 873 |  |  | 312 |  |  | 454 |  |  | 853 |  |
| Travel Time（s） |  | 14.9 |  |  | 5.3 |  |  | 7.7 |  |  | 14.5 |  |
| Confl．Peds．（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ |
| Heavy Vehicles（\％） | 3\％ | 4\％ | 5\％ | 6\％ | 1\％ | 5\％ | 7\％ | 7\％ | 7\％ | 6\％ | 7\％ | 0\％ |
| Bus Blockages（\＃／hr） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid－Block Traffic（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 61 | 593 | 540 | 114 | 863 | 0 | 279 | 1448 | 0 | 530 | 1174 | 39 |
| Turn Type | pm＋pt | NA | pm＋ov | pm＋pt | NA |  | Prot | NA |  | Prot | NA | pm＋ov |
| Protected Phases | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Permitted Phases | 4 |  | 4 | 8 |  |  |  |  |  |  |  | 6 |
| Detector Phase | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 8.0 | 4.0 | 3.0 | 8.0 |  | 4.0 | 15.0 |  | 4.0 | 15.0 | 3.0 |
| Minimum Split（s） | 6.5 | 14.0 | 8.5 | 6.5 | 14.0 |  | 8.5 | 21.0 |  | 8.5 | 43.0 | 6.5 |
| Total Split（s） | 14.0 | 31.0 | 21.0 | 14.0 | 31.0 |  | 21.0 | 52.0 |  | 28.0 | 59.0 | 14.0 |
| Total Split（\％） | 11．2\％ | 24．8\％ | 16．8\％ | 11．2\％ | 24．8\％ |  | 16．8\％ | 41．6\％ |  | 22．4\％ | 47．2\％ | 11．2\％ |
| Yellow Time（s） | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 |  | 3.5 | 4.5 |  | 3.5 | 4.5 | 3.5 |
| All－Red Time（s） | 0.0 | 1.5 | 1.0 | 0.0 | 1.5 |  | 1.0 | 1.5 |  | 1.0 | 1.5 | 0.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.5 | 6.0 | 4.5 | 3.5 | 6.0 |  | 4.5 | 6.0 |  | 4.5 | 6.0 | 3.5 |
| Lead／Lag | Lead | Lag | Lead | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lead |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None |  | None | C－Min |  | None | C－Min | None |
| Act Effct Green（s） | 35.5 | 24.7 | 46.0 | 38.7 | 28.0 |  | 15.3 | 47.6 |  | 23.0 | 55.2 | 69.6 |
| Actuated g／C Ratio | 0.28 | 0.20 | 0.37 | 0.31 | 0.22 |  | 0.12 | 0.38 |  | 0.18 | 0.44 | 0.56 |


|  | $\stackrel{ }{*}$ |  |  |  |  |  |  | $\dagger$ |  | * | $\frac{1}{7}$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.34 | 0.82 | 0.86 | 0.57 | 0.92dr |  | 0.72 | 1.14 |  | 0.90 | 0.77 | 0.04 |
| Control Delay | 34.5 | 58.6 | 44.8 | 41.9 | 40.7 |  | 63.8 | 109.1 |  | 69.9 | 34.5 | 1.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.5 | 58.6 | 44.8 | 41.9 | 40.7 |  | 63.8 | 109.1 |  | 69.9 | 34.5 | 1.2 |
| LOS | C | E | D | D | D |  | E | F |  | E | C | A |
| Approach Delay |  | 51.1 |  |  | 40.8 |  |  | 101.8 |  |  | 44.6 |  |
| Approach LOS |  | D |  |  | D |  |  | F |  |  | D |  |
| Queue Length 50th (tt) | 34 | 243 | 334 | 66 | 230 |  | 112 | $\sim 737$ |  | 217 | 430 | 0 |
| Queue Length 95th (tt) | 67 | 311 | \#536 | 113 | \#369 |  | 159 | \#880 |  | \#311 | 523 | 7 |
| Internal Link Dist (tt) |  | 793 |  |  | 232 |  |  | 374 |  |  | 773 |  |
| Turn Bay Length (tt) | 190 |  | 275 | 300 |  |  | 460 |  |  | 500 |  | 640 |
| Base Capacity (vph) | 209 | 734 | 639 | 208 | 969 |  | 417 | 1270 |  | 600 | 1516 | 923 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.29 | 0.81 | 0.85 | 0.55 | 0.89 |  | 0.67 | 1.14 |  | 0.88 | 0.77 | 0.04 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 125 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 125 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 72 (58\%), Referenced to phase 2:NBT and 6:SBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.14 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 62.8 |  |  |  |  | Intersection LOS: E |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 99.3\% |  |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

dr Defacto Right Lane. Recode with 1 though lane as a right lane.
Splits and Phases: 1: Milwaukee Avenue \& Deerfield Road


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | +4 | 「 |  | 中 ${ }^{\text {a }}$ |  |  |  | F |  | \& |  |
| Traffic Vol, veh/h | 3 | 1154 | 65 | 0 | 935 | 8 | 0 | 0 | 34 | 2 | 0 | 2 |
| Future Vol, veh/h | 3 | 1154 | 65 | 0 | 935 | 8 | 0 | 0 | 34 | 2 | 0 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | Free | - | - | None | - | - | Stop | - | - | None |
| Storage Length | - | - | 185 | - | - | - | - | - | 0 | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 | 95 | 95 | 95 | 96 | 95 | 96 |
| Heavy Vehicles, \% | 33 | 5 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 3 | 1202 | 68 | 0 | 974 | 8 | 0 | 0 | 36 | 2 | 0 | 2 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.6 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | $\neq$ | $\uparrow$ |  | Mr |  |
| Traffic Vol, veh/h | 3 | 1180 | 933 | 4 | 11 | 5 |
| Future Vol, veh/h | 3 | 1180 | 933 | 4 | 11 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 5 | 3 | 0 | 0 | 0 |
| Mvmt Flow | 3 | 1242 | 982 | 4 | 12 | 5 |


| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 986 | 0 | - | 0 | 2232 | 984 |
| Stage 1 | - | - | - | - | 984 | - |
| Stage 2 | - | - | - | - | 1248 | - |
| Critical Hdwy | 4.1 | - | - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 709 | - | - | - | 48 | 304 |
| $\quad$ Stage 1 | - | - | - | - | 365 | - |
| Stage 2 | - | - | - | - | 273 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 709 | - | - | - | 47 | 304 |
| Mov Cap-2 Maneuver | - | - | - | - | 47 | - |
| Stage 1 | - | - | - | - | 360 | - |
| Stage 2 | - | - | - | - | 273 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 80.3 |
| HCM LOS |  | $F$ |  |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 709 | - | - | - |

Capacity Analysis Summary Sheets No-Build Weekday Evening Peak Hour Conditions

|  | 4 | $\rightarrow$ |  | 7 | $\downarrow$ |  | $4$ | $\dagger$ | $p$ | $v$ | $\frac{1}{\dagger}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 44 | T | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  | \％ | 中 ${ }^{\text {a }}$ |  | ${ }^{1 *}$ | 44 | 「 |
| Traffic Volume（vph） | 109 | 316 | 340 | 116 | 794 | 330 | 424 | 1451 | 41 | 461 | 1447 | 66 |
| Future Volume（vph） | 109 | 316 | 340 | 116 | 794 | 330 | 424 | 1451 | 41 | 461 | 1447 | 66 |
| Ideal Flow（vphpl） | 1900 | 2000 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 2000 | 1900 |
| Lane Width（ft） | 12 | 12 | 12 | 12 | 12 | 12 | 11 | 12 | 12 | 11 | 11 | 11 |
| Grade（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Storage Length（ft） | 190 |  | 275 | 300 |  | 0 | 460 |  | 0 | 500 |  | 640 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 2 |  | 0 | 2 |  | 1 |
| Taper Length（ft） | 190 |  |  | 125 |  |  | 300 |  |  | 300 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.95 | 0.97 | 0.95 | 0.95 | 0.97 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  | 0.850 |  | 0.956 |  |  | 0.996 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 3762 | 1568 | 1770 | 3355 | 0 | 3286 | 3492 | 0 | 3319 | 3566 | 1561 |
| Flt Permitted | 0.122 |  |  | 0.488 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（perm） | 227 | 3762 | 1568 | 909 | 3355 | 0 | 3286 | 3492 | 0 | 3319 | 3566 | 1561 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 101 |  | 46 |  |  | 2 |  |  |  | 63 |
| Link Speed（mph） |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance（ft） |  | 873 |  |  | 312 |  |  | 454 |  |  | 853 |  |
| Travel Time（s） |  | 14.9 |  |  | 5.3 |  |  | 7.7 |  |  | 14.5 |  |
| Confl．Peds．（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ |
| Heavy Vehicles（\％） | 2\％ | 1\％ | 3\％ | 2\％ | 2\％ | 5\％ | 3\％ | 3\％ | 2\％ | 2\％ | 3\％ | 0\％ |
| Bus Blockages（\＃／hr） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid－Block Traffic（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 111 | 322 | 347 | 118 | 1147 | 0 | 433 | 1523 | 0 | 470 | 1477 | 67 |
| Turn Type | pm＋pt | NA | pm＋ov | pm＋pt | NA |  | Prot | NA |  | Prot | NA | pm＋ov |
| Protected Phases | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Permitted Phases | 4 |  | 4 | 8 |  |  |  |  |  |  |  | 6 |
| Detector Phase | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 8.0 | 4.0 | 3.0 | 8.0 |  | 4.0 | 15.0 |  | 4.0 | 15.0 | 3.0 |
| Minimum Split（s） | 6.5 | 14.0 | 8.5 | 6.5 | 14.0 |  | 8.5 | 21.0 |  | 8.5 | 43.0 | 6.5 |
| Total Split（s） | 14.0 | 38.0 | 24.0 | 14.0 | 38.0 |  | 24.0 | 56.0 |  | 22.0 | 54.0 | 14.0 |
| Total Split（\％） | 10．8\％ | 29．2\％ | 18．5\％ | 10．8\％ | 29．2\％ |  | 18．5\％ | 43．1\％ |  | 16．9\％ | 41．5\％ | 10．8\％ |
| Yellow Time（s） | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 |  | 3.5 | 4.5 |  | 3.5 | 4.5 | 3.5 |
| All－Red Time（s） | 0.0 | 1.5 | 1.0 | 0.0 | 1.5 |  | 1.0 | 1.5 |  | 1.0 | 1.5 | 0.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.5 | 6.0 | 4.5 | 3.5 | 6.0 |  | 4.5 | 6.0 |  | 4.5 | 6.0 | 3.5 |
| Lead／Lag | Lead | Lag | Lead | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lead |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None |  | None | C－Min |  | None | C－Min | None |
| Act Effct Green（s） | 45.2 | 32.7 | 57.9 | 44.8 | 32.6 |  | 19.2 | 50.0 |  | 17.5 | 48.3 | 64.3 |
| Actuated g／C Ratio | 0.35 | 0.25 | 0.45 | 0.34 | 0.25 |  | 0.15 | 0.38 |  | 0.13 | 0.37 | 0.49 |


|  | $\psi$ |  |  | $\checkmark$ |  |  | 4 | 9 | \% |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.57 | 0.34 | 0.46 | 0.31 | 1.31 |  | 0.90 | 1.13 |  | 1.05 | 1.11 | 0.08 |
| Control Delay | 39.0 | 41.2 | 19.6 | 29.9 | 186.3 |  | 76.3 | 107.0 |  | 110.8 | 100.7 | 4.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay | 39.0 | 41.2 | 19.6 | 29.9 | 186.3 |  | 76.3 | 107.0 |  | 110.8 | 100.7 | 4.8 |
| LOS | D | D | B | C | F |  | E | F |  | F | F | A |
| Approach Delay |  | 31.3 |  |  | 171.7 |  |  | 100.2 |  |  | 99.9 |  |
| Approach LOS |  | C |  |  | F |  |  | F |  |  | F |  |
| Queue Length 50th (ft) | 62 | 118 | 141 | 66 | $\sim 647$ |  | 186 | $\sim 785$ |  | $\sim 222$ | $\sim 754$ | 2 |
| Queue Length 95th (ft) | 106 | 162 | 226 | 112 | \#787 |  | \#275 | \#928 |  | \#332 | \#894 | 26 |
| Internal Link Dist (ft) |  | 793 |  |  | 232 |  |  | 374 |  |  | 773 |  |
| Turn Bay Length (ft) | 190 |  | 275 | 300 |  |  | 460 |  |  | 500 |  | 640 |
| Base Capacity (vph) | 204 | 947 | 757 | 388 | 874 |  | 492 | 1344 |  | 446 | 1325 | 810 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.54 | 0.34 | 0.46 | 0.30 | 1.31 |  | 0.88 | 1.13 |  | 1.05 | 1.11 | 0.08 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 33 (25\%), Referenced to phase 2:NBT and 6:SBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.31 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 106.2 |  |  |  |  | Intersection LOS: F |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 110.2\% |  |  |  |  | ICU Level of Service H |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Milwaukee Avenue \& Deerfield Road


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.9 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | +4 | 「 |  | 中 ${ }^{\text {a }}$ |  |  |  | F |  | \& |  |
| Traffic Vol, veh/h | 2 | 750 | 66 | 0 | 1219 | 11 | 0 | 0 | 30 | 13 | 0 | 21 |
| Future Vol, veh/h | 2 | 750 | 66 | 0 | 1219 | 11 | 0 | 0 | 30 | 13 | 0 | 21 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | Free | - | - | None | - | - | Stop | - | - | None |
| Storage Length | - | - | 185 | - | - | - | - | - | 0 | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 2 | 789 | 69 | 0 | 1283 | 12 | 0 | 0 | 32 | 14 | 0 | 22 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 1.7 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 4 | 「 | * | $\hat{\beta}$ |  | ${ }^{7}$ | $\uparrow$ |  |  | * |  |
| Traffic Vol, veh/h | 1 | 781 | 11 | 27 | 1177 | 0 | 53 | 0 | 15 | 0 | 0 | 0 |
| Future Vol, veh/h | 1 | 781 | 11 | 27 | 1177 | 0 | 53 | 0 | 15 | 0 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 117 | - | - | 185 | - | - | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 1 | - | - | 1 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 | 93 |
| Heavy Vehicles, \% | 0 | 2 | 0 | 0 | 3 | 0 | 0 | 0 | 22 | 0 | 0 | 0 |
| Mvmt Flow | 1 | 840 | 12 | 29 | 1266 | 0 | 57 | 0 | 16 | 0 | 0 | 0 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1477 | 0 | - | 0 | 2447 | 1470 |
| Stage 1 | - | - | - | - | 1470 | - |
| Stage 2 | - | - | - | - | 977 | - |
| Critical Hdwy | 4.1 | - | - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 462 | - | - | - | 35 | 158 |
| Stage 1 | - |  | - | - | 213 | - |
| Stage 2 | - | - | - | - | 368 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 462 | - | - | - | 34 | 158 |
| Mov Cap-2 Maneuver | - | - | - | - | 34 | - |
| Stage 1 | - |  | - | - | 207 | - |
| Stage 2 | - | - | - | - | 368 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.1 |  | 0 |  | 78 |  |
| HCM LOS |  |  |  |  | F |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR | SBLn1 |
| Capacity (veh/h) |  | 462 | - | - | - | 60 |
| HCM Lane V/C Ratio |  | 0.013 | - | - | - | 0.183 |
| HCM Control Delay (s) |  | 12.9 | 0 |  | - | 78 |
| HCM Lane LOS |  | B | A | - | - | F |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 0.6 |

## Capacity Analysis Summary Sheets <br> Projected Weekday Morning Peak Hour Conditions

|  | 4 | $\rightarrow$ |  | 4 |  |  |  | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 44 | 7 | ${ }^{7}$ | 車 $\hat{p}$ |  | 7 | 中 $\hat{p}$ |  | ${ }^{7} 1$ | 中4 | F |
| Traffic Volume（vph） | 59 | 568 | 518 | 115 | 289 | 548 | 268 | 1246 | 147 | 511 | 1127 | 37 |
| Future Volume（vph） | 59 | 568 | 518 | 115 | 289 | 548 | 268 | 1246 | 147 | 511 | 1127 | 37 |
| Ideal Flow（vphpl） | 1900 | 2000 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 2000 | 1900 |
| Lane Width（ft） | 12 | 12 | 12 | 12 | 12 | 12 | 11 | 12 | 12 | 11 | 11 | 11 |
| Grade（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Storage Length（ft） | 190 |  | 275 | 300 |  | 0 | 460 |  | 0 | 500 |  | 640 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 2 |  | 0 | 2 |  | 1 |
| Taper Length（ft） | 190 |  |  | 125 |  |  | 300 |  |  | 300 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.95 | 0.97 | 0.95 | 0.95 | 0.97 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  | 0.850 |  | 0.902 |  |  | 0.984 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1752 | 3654 | 1538 | 1703 | 3142 | 0 | 3164 | 3320 | 0 | 3193 | 3433 | 1561 |
| Flt Permitted | 0.158 |  |  | 0.160 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（perm） | 291 | 3654 | 1538 | 287 | 3142 | 0 | 3164 | 3320 | 0 | 3193 | 3433 | 1561 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 96 |  | 343 |  |  | 11 |  |  |  | 65 |
| Link Speed（mph） |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance（ft） |  | 873 |  |  | 312 |  |  | 454 |  |  | 853 |  |
| Travel Time（s） |  | 14.9 |  |  | 5.3 |  |  | 7.7 |  |  | 14.5 |  |
| Confl．Peds．（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ |
| Heavy Vehicles（\％） | 3\％ | 4\％ | 5\％ | 6\％ | 1\％ | 5\％ | 7\％ | 7\％ | 7\％ | 6\％ | 7\％ | 0\％ |
| Bus Blockages（\＃／hr） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid－Block Traffic（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 61 | 592 | 540 | 120 | 872 | 0 | 279 | 1451 | 0 | 532 | 1174 | 39 |
| Turn Type | pm＋pt | NA | pm＋ov | pm＋pt | NA |  | Prot | NA |  | Prot | NA | pm＋ov |
| Protected Phases | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Permitted Phases | 4 |  | 4 | 8 |  |  |  |  |  |  |  | 6 |
| Detector Phase | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 8.0 | 4.0 | 3.0 | 8.0 |  | 4.0 | 15.0 |  | 4.0 | 15.0 | 3.0 |
| Minimum Split（s） | 6.5 | 14.0 | 8.5 | 6.5 | 14.0 |  | 8.5 | 21.0 |  | 8.5 | 43.0 | 6.5 |
| Total Split（s） | 14.0 | 31.0 | 21.0 | 14.0 | 31.0 |  | 21.0 | 52.0 |  | 28.0 | 59.0 | 14.0 |
| Total Split（\％） | 11．2\％ | 24．8\％ | 16．8\％ | 11．2\％ | 24．8\％ |  | 16．8\％ | 41．6\％ |  | 22．4\％ | 47．2\％ | 11．2\％ |
| Yellow Time（s） | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 |  | 3.5 | 4.5 |  | 3.5 | 4.5 | 3.5 |
| All－Red Time（s） | 0.0 | 1.5 | 1.0 | 0.0 | 1.5 |  | 1.0 | 1.5 |  | 1.0 | 1.5 | 0.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.5 | 6.0 | 4.5 | 3.5 | 6.0 |  | 4.5 | 6.0 |  | 4.5 | 6.0 | 3.5 |
| Lead／Lag | Lead | Lag | Lead | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lead |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None |  | None | C－Min |  | None | C－Min | None |
| Act Effct Green（s） | 35.5 | 24.6 | 45.9 | 38.8 | 28.0 |  | 15.3 | 47.5 |  | 23.0 | 55.2 | 69.5 |
| Actuated g／C Ratio | 0.28 | 0.20 | 0.37 | 0.31 | 0.22 |  | 0.12 | 0.38 |  | 0.18 | 0.44 | 0.56 |


|  | $\stackrel{ }{*}$ |  |  |  |  |  |  | $\dagger$ |  |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.34 | 0.82 | 0.86 | 0.60 | 0.94dr |  | 0.72 | 1.14 |  | 0.91 | 0.77 | 0.04 |
| Control Delay | 34.5 | 58.7 | 45.0 | 43.3 | 41.9 |  | 63.8 | 110.6 |  | 70.3 | 34.6 | 1.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay | 34.5 | 58.7 | 45.0 | 43.3 | 41.9 |  | 63.8 | 110.6 |  | 70.3 | 34.6 | 1.2 |
| LOS | C | E | D | D | D |  | E | F |  | E | C | A |
| Approach Delay |  | 51.3 |  |  | 42.0 |  |  | 103.1 |  |  | 44.7 |  |
| Approach LOS |  | D |  |  | D |  |  | F |  |  | D |  |
| Queue Length 50th (ft) | 34 | 242 | 334 | 69 | 235 |  | 112 | $\sim 740$ |  | 218 | 430 | 0 |
| Queue Length 95th (tt) | 67 | 311 | \#536 | 119 | \#379 |  | 159 | \#881 |  | \#313 | 523 | 7 |
| Internal Link Dist (tt) |  | 793 |  |  | 232 |  |  | 374 |  |  | 773 |  |
| Turn Bay Length (t) | 190 |  | 275 | 300 |  |  | 460 |  |  | 500 |  | 640 |
| Base Capacity (vph) | 210 | 732 | 639 | 208 | 969 |  | 417 | 1268 |  | 600 | 1515 | 922 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.29 | 0.81 | 0.85 | 0.58 | 0.90 |  | 0.67 | 1.14 |  | 0.89 | 0.77 | 0.04 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 125 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 125 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 72 (58\%), Referenced to phase 2:NBT and 6:SBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 100 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.14 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 63.5 |  |  |  |  | Intersection LOS: E |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 99.8\% |  |  |  |  | ICU Level of Service F |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

dr Defacto Right Lane. Recode with 1 though lane as a right lane.
Splits and Phases: 1: Milwaukee Avenue \& Deerfield Road


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.3 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢4 | F' |  | 中 ${ }^{\text {a }}$ |  |  |  | 7 |  | $\uparrow$ |  |
| Traffic Vol, veh/h | 3 | 1158 | 65 | 0 | 950 | 8 | 0 | 0 | 34 | 2 | 0 | 2 |
| Future Vol, veh/h | 3 | 1158 | 65 | 0 | 950 | 8 | 0 | 0 | 34 | 2 | 0 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | Free | - | - | None | - | - | Stop | - | - | None |
| Storage Length | - | - | 185 | - | - | - | - | - | 0 | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 | 95 | 95 | 95 | 96 | 95 | 96 |
| Heavy Vehicles, \% | 33 | 5 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 3 | 1206 | 68 | 0 | 990 | 8 | 0 | 0 | 36 | 2 | 0 | 2 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |  |  |  |  |  |  |  |


| Major/Minor | Major1 | Major2 |  |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1019 | 0 | 0 | 1322 | , | 0 | 2406 | 2401 | 1314 | 2407 | 2409 | 1019 |
| Stage 1 | - | - | - | - | - | - | 1322 | 1322 | - | 1079 | 1079 | - |
| Stage 2 | - | - | - | - | - | - | 1084 | 1079 | - | 1328 | 1330 | - |
| Critical Hdwy | 4.1 | - | - | 4.1 | - | - | 7.1 | 6.5 | 6.2 | 7.1 | 6.5 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.1 | 5.5 | - | 6.1 | 5.5 | - |
| Follow-up Hdwy | 2.2 | - | - | 2.2 | - | - | 3.5 | 4 | 3.3 | 3.5 | 4 | 3.3 |
| Pot Cap-1 Maneuver | 689 | - | - | 529 | - | - | ~23 | 34 | 195 | 23 | 33 | 290 |
| Stage 1 | - | - | - | - | - | - | 195 | 228 | - | 267 | 297 | - |
| Stage 2 | - | - | - | - | - | - | 265 | 297 | - | 193 | 226 | - |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 689 | - | - | 529 | - | - | ~21 | 32 | 195 | 22 | 31 | 290 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | 107 | 128 | - | 100 | 119 | - |
| Stage 1 | - | - | - | - | - | - | 194 | 227 | - | 265 | 280 | - |
| Stage 2 | - | - | - | - | - | - | 241 | 280 | - | 189 | 225 | - |


| Approach | EB | WB | NB | SB |
| :--- | :---: | :---: | :---: | :---: |
| HCM Control Delay, s | 0 | 0.3 | 52.7 | 22.2 |
| HCM LOS |  | F | C |  |


|  | Minor Lane/Major Mvmt | NBLn1 NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 SBLn2 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 107 | 195 | 689 | - | -529 | - | -100 | 290 |  |
| HCM Lane V/C Ratio | 0.343 | 0.017 | 0.006 | - | -0.057 | - | -0.022 | 0.034 |  |
| HCM Control Delay (s) | 55.3 | 23.8 | 10.3 | - | - | 12.2 | - | - | 41.8 |
| 17.9 |  |  |  |  |  |  |  |  |  |
| HCM Lane LOS | F | C | B | - | - | B | - | - | E |
| HCM 95th \%tatle Q(veh) | 1.4 | 0.1 | 0 | - | - | 0.2 | - | - | 0.1 |

## Notes

```
~: Volume exceeds capacity $: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon
```



| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | :--- | :--- | :--- | ---: | ---: |
| Conflicting Flow All | 988 | 0 | - | 0 | 2241 | 988 |
| Stage 1 | - | - | - | - | 988 | - |
| Stage 2 | - | - | - | - | 1253 | - |
| Critical Hdwy | 4.1 | - | - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 708 | - | - | - | 47 | 303 |
| $\quad$ Stage 1 | - | - | - | - | 364 | - |
| Stage 2 | - | - | - | - | 272 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 708 | - | - | - | 46 | 303 |
| Mov Cap-2 Maneuver | - | - | - | - | 46 | - |
| Stage 1 | - | - | - | - | 359 | - |
| Stage 2 | - | - | - | - | 272 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 48.1 |
| HCM LOS |  | E |  |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 708 | - | - | - |
| HCM Lane V/C Ratio | 0.004 | - | - | -0.112 |
| HCM Control Delay (s) | 10.1 | 0 | - | -48.1 |
| HCM Lane LOS | B | A | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor $\quad$ N | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 987 | 0 | - | 0 | 2239 | 985 |
| Stage 1 | - | - | - | - | 985 | - |
| Stage 2 | - | - | - | - | 1254 | - |
| Critical Hdwy | 4.1 | - | - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 708 | - | - | - | 47 | 304 |
| Stage 1 | - | - | - | - | 365 | - |
| Stage 2 | - | - | - |  | 271 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 708 | - | - | - | 46 | 304 |
| Mov Cap-2 Maneuver | - |  | - | - | 46 | - |
| Stage 1 | - | - | - |  | 360 | - |
| Stage 2 | - | - | - | - | 271 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0 |  | 0 |  | 81.8 |  |
| HCM LOS |  |  |  |  | F |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR | SBLn1 |
| Capacity (veh/h) |  | 708 | - |  | - | 63 |
| HCM Lane V/C Ratio |  | 0.004 | - | - | - | 0.267 |
| HCM Control Delay (s) |  | 10.1 | 0 | - | - | 81.8 |
| HCM Lane LOS |  | B | A | - | - | F |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 0.9 |


|  | 4 | $\rightarrow$ |  | 4 |  |  | 4 | 4 | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | $\cdots$ | 44 | 7 | \％ | 种4 | 「 | \％ | 44 | 「 | ${ }^{7} 1$ | 中4 | F |
| Traffic Volume（vph） | 62 | 565 | 518 | 115 | 289 | 548 | 268 | 1246 | 147 | 513 | 1127 | 37 |
| Future Volume（vph） | 62 | 565 | 518 | 115 | 289 | 548 | 268 | 1246 | 147 | 513 | 1127 | 37 |
| Ideal Flow（vphpl） | 1900 | 2000 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 2000 | 1900 |
| Lane Width（ft） | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 12 | 12 | 11 | 11 | 11 |
| Grade（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Storage Length（ft） | 220 |  | 520 | 285 |  | 480 | 450 |  | 480 | 485 |  | 600 |
| Storage Lanes | 2 |  | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  | 1 |
| Taper Length（ft） | 216 |  |  | 270 |  |  | 300 |  |  | 299 |  |  |
| Lane Util．Factor | 0.97 | 0.95 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 3286 | 3532 | 1487 | 3193 | 4964 | 1487 | 3164 | 3374 | 1509 | 3193 | 3433 | 1561 |
| Flt Permitted | 0.561 |  |  | 0.187 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（perm） | 1941 | 3532 | 1487 | 629 | 4964 | 1487 | 3164 | 3374 | 1509 | 3193 | 3433 | 1561 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 100 |  |  | 156 |  |  | 109 |  |  | 68 |
| Link Speed（mph） |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance（ft） |  | 873 |  |  | 308 |  |  | 454 |  |  | 853 |  |
| Travel Time（s） |  | 14.9 |  |  | 5.3 |  |  | 7.7 |  |  | 14.5 |  |
| Confl．Peds．（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 | 0.96 |
| Growth Factor | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ |
| Heavy Vehicles（\％） | 3\％ | 4\％ | 5\％ | 6\％ | 1\％ | 5\％ | 7\％ | 7\％ | 7\％ | 6\％ | 7\％ | 0\％ |
| Bus Blockages（\＃／hr） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid－Block Traffic（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 65 | 589 | 540 | 120 | 301 | 571 | 279 | 1298 | 153 | 534 | 1174 | 39 |
| Turn Type | pm＋pt | NA | pm＋ov | pm＋pt | NA | pm＋ov | Prot | NA | pm＋ov | Prot | NA | pm＋ov |
| Protected Phases | 7 | 4 | 5 | 3 | 8 | 1 | 5 | 2 | 3 | 1 | 6 | 7 |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 |  |  | 2 |  |  | 6 |
| Detector Phase | 7 | 4 | 5 | 3 | 8 | 1 | 5 | 2 | 3 | 1 | 6 | 7 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 8.0 | 4.0 | 3.0 | 8.0 | 4.0 | 4.0 | 15.0 | 3.0 | 4.0 | 15.0 | 3.0 |
| Minimum Split（s） | 6.5 | 14.0 | 8.5 | 6.5 | 14.0 | 8.5 | 8.5 | 21.0 | 6.5 | 8.5 | 43.0 | 6.5 |
| Total Split（s） | 14.0 | 31.0 | 20.0 | 14.0 | 31.0 | 27.0 | 20.0 | 48.0 | 14.0 | 27.0 | 55.0 | 14.0 |
| Total Split（\％） | 11．7\％ | 25．8\％ | 16．7\％ | 11．7\％ | 25．8\％ | 22．5\％ | 16．7\％ | 40．0\％ | 11．7\％ | 22．5\％ | 45．8\％ | 11．7\％ |
| Yellow Time（s） | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 | 3.5 |
| All－Red Time（s） | 0.0 | 1.5 | 1.0 | 0.0 | 1.5 | 1.0 | 1.0 | 1.5 | 0.0 | 1.0 | 1.5 | 0.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.5 | 6.0 | 4.5 | 3.5 | 6.0 | 4.5 | 4.5 | 6.0 | 3.5 | 4.5 | 6.0 | 3.5 |
| Lead／Lag | Lead | Lag | Lead | Lead | Lag | Lead | Lead | Lag | Lead | Lead | Lag | Lead |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | None | C－Min | None | None | C－Min | None |
| Act Effct Green（s） | 34.9 | 25.3 | 45.9 | 38.3 | 28.6 | 57.2 | 14.6 | 43.6 | 58.1 | 22.6 | 51.6 | 64.6 |
| Actuated g／C Ratio | 0.29 | 0.21 | 0.38 | 0.32 | 0.24 | 0.48 | 0.12 | 0.36 | 0.48 | 0.19 | 0.43 | 0.54 |

Projected Morning Peak－W／Roadway Improvements Townhomes－Riverwoods 10：33 am 12／14／2021 21－108 ANB

Synchro 11 Report Page 1

|  | 4 |  |  | $\checkmark$ |  |  |  | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.10 | 0.79 | 0.86 | 0.31 | 0.25 | 0.72 | 0.73 | 1.06 | 0.19 | 0.89 | 0.80 | 0.04 |
| Control Delay | 27.0 | 53.5 | 42.0 | 29.5 | 38.1 | 24.2 | 62.3 | 80.6 | 6.5 | 65.7 | 35.3 | 1.1 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 27.0 | 53.5 | 42.0 | 29.5 | 38.1 | 24.2 | 62.3 | 80.6 | 6.5 | 65.7 | 35.3 | 1.1 |
| LOS | C | D | D | C | D | C | E | F | A | E | D | A |
| Approach Delay |  | 46.8 |  |  | 29.1 |  |  | 71.1 |  |  | 43.9 |  |
| Approach LOS |  | D |  |  | C |  |  | E |  |  | D |  |
| Queue Length 50th (ft) | 17 | 224 | 308 | 32 | 69 | 256 | 107 | ~600 | 18 | 209 | 423 | 0 |
| Queue Length 95th (ft) | 33 | 297 | \#523 | 54 | 99 | 414 | 155 | \#738 | 54 | \#306 | 518 | 6 |
| Internal Link Dist (ft) |  | 793 |  |  | 228 |  |  | 374 |  |  | 773 |  |
| Turn Bay Length (ft) | 220 |  | 520 | 285 |  | 480 | 450 |  | 480 | 485 |  | 600 |
| Base Capacity (vph) | 736 | 761 | 641 | 430 | 1183 | 793 | 408 | 1225 | 810 | 607 | 1475 | 914 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.09 | 0.77 | 0.84 | 0.28 | 0.25 | 0.72 | 0.68 | 1.06 | 0.19 | 0.88 | 0.80 | 0.04 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 72 (60\%), Referenced to phase 2:NBT and 6:SBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 90 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.06 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 50.2 |  |  |  |  | Intersection LOS: D |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 84.3\% |  |  |  |  | ICU Level of Service E |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Milwaukee Avenue \& Deerfield Road


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 44 | 「 |  | 虾 |  |  |  | F |  |  | F' |
| Traffic Vol, veh/h | 0 | 1160 | 65 | 0 | 950 | 8 | 0 | 0 | 34 | 0 | 0 | 2 |
| Future Vol, veh/h | 0 | 1160 | 65 | 0 | 950 | 8 | 0 | 0 | 34 | 0 | 0 | 2 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | Stop | - | - | None |
| Storage Length | - | - | 0 | - | - | - | - | - | 0 | - | - | 0 |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 | 96 |
| Heavy Vehicles, \% | 33 | 5 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 1208 | 68 | 0 | 990 | 8 | 0 | 0 | 35 | 0 | 0 | 2 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \＃ | 个 ${ }^{\text {F }}$ |  |  | 虾 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 个 |  | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Vol，veh／h | 7 | 1180 | 7 | 27 | 916 | 1 | 33 | 0 | 3 | 6 | 0 | 9 |
| Future Vol，veh／h | 7 | 1180 | 7 | 27 | 916 | 1 | 33 | 0 | 3 | 6 | 0 | 9 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | 117 | － | － | 185 | － | － | 0 | － | － | 0 | － | － |
| Veh in Median Storage，\＃ | － | 0 | － | － | 0 | － | － | 1 | － | － | 1 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles，\％ | 0 | 5 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 8 | 1311 | 8 | 30 | 1018 | 1 | 37 | 0 | 3 | 7 | 0 | 10 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations |  | 个4 | 作 |  |  | $\mathbf{7}$ |
| Traffic Vol, veh/h | 0 | 1189 | 938 | 1 | 0 | 6 |
| Future Vol, veh/h | 0 | 1189 | 938 | 1 | 0 | 6 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | Free | - | Stop |
| Storage Length | - | - | - | - | - | 0 |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, $\%$ | 0 | 5 | 3 | 0 | 0 | 0 |
| Mvmt Flow | 0 | 1252 | 987 | 1 | 0 | 6 |


| Major/Minor |  | Major1 | Major2 |  | Minor2 |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | - | 0 | - | 0 | - | 494 |
| $\quad$ Stage 1 | - | - | - | - | - | - |
| $\quad$ Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | - | - | - | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | - | - | - | 3.3 |
| Pot Cap-1 Maneuver | 0 | - | - | 0 | 0 | 526 |
| $\quad$ Stage 1 | 0 | - | - | 0 | 0 | - |
| $\quad$ Stage 2 | 0 | - | - | 0 | 0 | - |
| Platoon blocked, \% |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | - | - | - | 526 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
|  |  |  |  |  |  |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 11.9 |
| HCM LOS |  | $B$ |  |


| Minor Lane/Major Mvmt | EBT | WBT SBLn1 |
| :--- | :---: | ---: |
| Capacity (veh/h) | - | -526 |
| HCM Lane V/C Ratio | - | -0.012 |
| HCM Control Delay (s) | - | -11.9 |
| HCM Lane LOS | - | - |
| HCM 95th \%tile Q(veh) | - | - |



| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | :--- | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 987 | 0 | - | 0 | 2239 | 494 |
| $\quad$ Stage 1 | - | - | - | - | 985 | - |
| $\quad$ Stage 2 | - | - | - | - | 1254 | - |
| Critical Hdwy | 4.1 | - | - | - | 6.6 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.8 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 708 | - | - | - | 42 | 526 |
| $\quad$ Stage 1 | - | - | - | - | 327 | - |
| $\quad$ Stage 2 | - | - | - | - | 271 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 708 | - | - | - | 42 | 526 |
| Mov Cap-2 Maneuver | - | - | - | - | 154 | - |
| Stage 1 | - | - | - | - | 326 | - |
| Stage 2 | - | - | - | - | 271 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 24.9 |
| HCM LOS |  |  | C |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 708 | - | - | -198 |
| HCM Lane V/C Ratio | 0.004 | - | - | -0.085 |
| HCM Control Delay (s) | 10.1 | - | - | -24.9 |
| HCM Lane LOS | B | - | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | - | - |
| C | 0.3 |  |  |  |

## Capacity Analysis Summary Sheets Projected Weekday Evening Peak Hour Conditions

|  | 4 |  | $\geqslant$ | 7 |  |  |  | $\dagger$ | \％ | $1$ | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 44 | 「 | ${ }^{7}$ | 中 $\%$ |  | 4 | 中 ${ }^{\text {a }}$ |  | 4 | 44 | F＇ |
| Traffic Volume（vph） | 109 | 318 | 340 | 121 | 796 | 336 | 424 | 1451 | 47 | 467 | 1447 | 66 |
| Future Volume（vph） | 109 | 318 | 340 | 121 | 796 | 336 | 424 | 1451 | 47 | 467 | 1447 | 66 |
| Ideal Flow（vphpl） | 1900 | 2000 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 2000 | 1900 |
| Lane Width（ft） | 12 | 12 | 12 | 12 | 12 | 12 | 11 | 12 | 12 | 11 | 11 | 11 |
| Grade（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Storage Length（ft） | 190 |  | 275 | 300 |  | 0 | 460 |  | 0 | 500 |  | 640 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 2 |  | 0 | 2 |  | 1 |
| Taper Length（ft） | 190 |  |  | 125 |  |  | 300 |  |  | 300 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 0.95 | 0.97 | 0.95 | 0.95 | 0.97 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  | 0.850 |  | 0.955 |  |  | 0.995 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 1770 | 3762 | 1568 | 1770 | 3351 | 0 | 3286 | 3488 | 0 | 3319 | 3566 | 1561 |
| Flt Permitted | 0.122 |  |  | 0.486 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（perm） | 227 | 3762 | 1568 | 905 | 3351 | 0 | 3286 | 3488 | 0 | 3319 | 3566 | 1561 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 98 |  | 48 |  |  | 3 |  |  |  | 63 |
| Link Speed（mph） |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance（ft） |  | 873 |  |  | 312 |  |  | 454 |  |  | 853 |  |
| Travel Time（s） |  | 14.9 |  |  | 5.3 |  |  | 7.7 |  |  | 14.5 |  |
| Confl．Peds．（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ |
| Heavy Vehicles（\％） | 2\％ | 1\％ | 3\％ | 2\％ | 2\％ | 5\％ | 3\％ | 3\％ | 2\％ | 2\％ | 3\％ | 0\％ |
| Bus Blockages（\＃／hr） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid－Block Traffic（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 111 | 324 | 347 | 123 | 1155 | 0 | 433 | 1529 | 0 | 477 | 1477 | 67 |
| Turn Type | pm＋pt | NA | pm＋ov | pm＋pt | NA |  | Prot | NA |  | Prot | NA | pm＋ov |
| Protected Phases | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Permitted Phases | 4 |  | 4 | 8 |  |  |  |  |  |  |  | 6 |
| Detector Phase | 7 | 4 | 5 | 3 | 8 |  | 5 | 2 |  | 1 | 6 | 7 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 8.0 | 4.0 | 3.0 | 8.0 |  | 4.0 | 15.0 |  | 4.0 | 15.0 | 3.0 |
| Minimum Split（s） | 6.5 | 14.0 | 8.5 | 6.5 | 14.0 |  | 8.5 | 21.0 |  | 8.5 | 43.0 | 6.5 |
| Total Split（s） | 14.0 | 38.0 | 24.0 | 14.0 | 38.0 |  | 24.0 | 56.0 |  | 22.0 | 54.0 | 14.0 |
| Total Split（\％） | 10．8\％ | 29．2\％ | 18．5\％ | 10．8\％ | 29．2\％ |  | 18．5\％ | 43．1\％ |  | 16．9\％ | 41．5\％ | 10．8\％ |
| Yellow Time（s） | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 |  | 3.5 | 4.5 |  | 3.5 | 4.5 | 3.5 |
| All－Red Time（s） | 0.0 | 1.5 | 1.0 | 0.0 | 1.5 |  | 1.0 | 1.5 |  | 1.0 | 1.5 | 0.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.5 | 6.0 | 4.5 | 3.5 | 6.0 |  | 4.5 | 6.0 |  | 4.5 | 6.0 | 3.5 |
| Lead／Lag | Lead | Lag | Lead | Lead | Lag |  | Lead | Lag |  | Lead | Lag | Lead |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes |  | Yes | Yes |  | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None |  | None | C－Min |  | None | C－Min | None |
| Act Effct Green（s） | 45.1 | 32.7 | 57.8 | 44.9 | 32.6 |  | 19.2 | 50.0 |  | 17.5 | 48.3 | 64.3 |
| Actuated g／C Ratio | 0.35 | 0.25 | 0.44 | 0.35 | 0.25 |  | 0.15 | 0.38 |  | 0.13 | 0.37 | 0.49 |


|  | $\psi$ |  |  | $\checkmark$ |  |  | 4 | 9 | \% |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.57 | 0.34 | 0.46 | 0.33 | 1.32 |  | 0.90 | 1.14 |  | 1.07 | 1.11 | 0.08 |
| Control Delay | 39.0 | 41.3 | 19.9 | 30.2 | 189.3 |  | 76.3 | 109.0 |  | 115.0 | 100.7 | 4.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 |
| Total Delay | 39.0 | 41.3 | 19.9 | 30.2 | 189.3 |  | 76.3 | 109.0 |  | 115.0 | 100.7 | 4.8 |
| LOS | D | D | B | C | F |  | E | F |  | F | F | A |
| Approach Delay |  | 31.5 |  |  | 174.0 |  |  | 101.8 |  |  | 100.9 |  |
| Approach LOS |  | C |  |  | F |  |  | F |  |  | F |  |
| Queue Length 50th (ft) | 62 | 118 | 142 | 69 | $\sim 654$ |  | 186 | ~791 |  | $\sim 228$ | $\sim 754$ | 2 |
| Queue Length 95th (ft) | 106 | 164 | 228 | 116 | \#794 |  | \#275 | \#933 |  | \#339 | \#894 | 26 |
| Internal Link Dist (ft) |  | 793 |  |  | 232 |  |  | 374 |  |  | 773 |  |
| Turn Bay Length (ft) | 190 |  | 275 | 300 |  |  | 460 |  |  | 500 |  | 640 |
| Base Capacity (vph) | 204 | 946 | 755 | 387 | 875 |  | 492 | 1343 |  | 446 | 1325 | 810 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.54 | 0.34 | 0.46 | 0.32 | 1.32 |  | 0.88 | 1.14 |  | 1.07 | 1.11 | 0.08 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 33 (25\%), Referenced to phase 2:NBT and 6:SBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 130 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.32 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 107.7 |  |  |  |  | Intersection LOS: F |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 110.8\% |  |  |  |  | ICU Level of Service H |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Milwaukee Avenue \& Deerfield Road


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 0.9 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | * 4 | F |  | 中\% |  |  |  | F |  | \$ |  |
| Traffic Vol, veh/h | 2 | 764 | 66 | 0 | 1232 | 11 | 0 | 0 | 30 | 13 | 0 | 21 |
| Future Vol, veh/h | 2 | 764 | 66 | 0 | 1232 | 11 | 0 | 0 | 30 | 13 | 0 | 21 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | Free | - | - | None | - | - | Stop | - | - | None |
| Storage Length | - | - | 185 | - | - | - | - | - | 0 | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 | 95 |
| Heavy Vehicles, \% | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Mvmt Flow | 2 | 804 | 69 | 0 | 1297 | 12 | 0 | 0 | 32 | 14 | 0 | 22 |






| Major/Minor M | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1273 | 0 | - | 0 | 2122 | 1271 |
| Stage 1 | - | - | - - | - | 1271 | - |
| Stage 2 | - | - | - - | - | 851 | - |
| Critical Hdwy | 4.1 | - | - - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - - | - | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 552 | - | - | - | 56 | 207 |
| Stage 1 | - | - | - - | - | 266 | - |
| Stage 2 | - | - | - | - | 422 | - |
| Platoon blocked, \% |  | - | - - | - |  |  |
| Mov Cap-1 Maneuver | 552 | - | - | - | 55 | 207 |
| Mov Cap-2 Maneuver | - | - | - - | - | 55 | - |
| Stage 1 | - | - | - | - | 261 | - |
| Stage 2 | - | - | - - | - | 422 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.1 |  | 0 |  | 38.1 |  |
| HCM LOS |  |  |  |  | E |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 552 |  | - | - | 116 |
| HCM Lane V/C Ratio |  | 0.011 | - | - | - | 0.064 |
| HCM Control Delay (s) |  | 11.6 | 0 | - |  | 38.1 |
| HCM Lane LOS |  | B | A | - | - | E |
| HCM 95th \%tile Q(veh) |  | 0 |  | - | - | 0.2 |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Major/Minor $\quad$ N | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1485 | 0 | - | 0 | 2458 | 1478 |
| Stage 1 | - | - | - |  | 1478 | - |
| Stage 2 | - | - | - | - | 980 |  |
| Critical Hdwy | 4.1 | - | - | - | 6.4 | 6.2 |
| Critical Hdwy Stg 1 | - | - | - |  | 5.4 | - |
| Critical Hdwy Stg 2 | - | - | - |  | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 459 | - | - | - | 34 | 156 |
| Stage 1 | - |  | - |  | 211 | - |
| Stage 2 | - | - | - |  | 367 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 459 | - | - | - | 33 | 156 |
| Mov Cap-2 Maneuver | - | - | - | - | 33 | - |
| Stage 1 | - | - | - | - | 205 | - |
| Stage 2 | - | - | - |  | 367 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.1 |  | 0 |  | 79.5 |  |
| HCM LOS |  |  |  |  | F |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 459 | - | - | - | 59 |
| HCM Lane V/C Ratio |  | 0.013 | - | - | - | 0.186 |
| HCM Control Delay (s) |  | 12.9 | 0 | - | - | 79.5 |
| HCM Lane LOS |  | B | A | - | - | F |
| HCM 95th \%tile Q(veh) |  | 0 | - |  |  | 0.6 |


|  | 4 |  | 7 | 7 |  |  |  | $\dagger$ | \％ | $1$ | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 中4 | 7 | ＊ | 种4 | 「 | ${ }^{*} 1$ | 中4 | 「＇ | 4 | 44 | F＇ |
| Traffic Volume（vph） | 111 | 316 | 340 | 121 | 796 | 336 | 424 | 1451 | 47 | 480 | 1447 | 66 |
| Future Volume（vph） | 111 | 316 | 340 | 121 | 796 | 336 | 424 | 1451 | 47 | 480 | 1447 | 66 |
| Ideal Flow（vphpl） | 1900 | 2000 | 1900 | 1900 | 2000 | 1900 | 1900 | 2000 | 1900 | 1900 | 2000 | 1900 |
| Lane Width（ft） | 11 | 11 | 11 | 11 | 11 | 11 | 11 | 12 | 12 | 11 | 11 | 11 |
| Grade（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Storage Length（ft） | 220 |  | 520 | 285 |  | 480 | 450 |  | 480 | 485 |  | 600 |
| Storage Lanes | 2 |  | 1 | 2 |  | 1 | 2 |  | 1 | 2 |  | 1 |
| Taper Length（ft） | 216 |  |  | 270 |  |  | 300 |  |  | 299 |  |  |
| Lane Util．Factor | 0.97 | 0.95 | 1.00 | 0.97 | 0.91 | 1.00 | 0.97 | 0.95 | 1.00 | 0.97 | 0.95 | 1.00 |
| Ped Bike Factor |  |  |  |  |  |  |  |  |  |  |  |  |
| Frt |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |  |  | 0.850 |
| Flt Protected | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（prot） | 3319 | 3637 | 1516 | 3319 | 5175 | 1487 | 3286 | 3689 | 1583 | 3319 | 3566 | 1561 |
| Flt Permitted | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  | 0.950 |  |  |
| Satd．Flow（perm） | 3319 | 3637 | 1516 | 3319 | 5175 | 1487 | 3286 | 3689 | 1583 | 3319 | 3566 | 1561 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd．Flow（RTOR） |  |  | 68 |  |  | 68 |  |  | 68 |  |  | 68 |
| Link Speed（mph） |  | 40 |  |  | 40 |  |  | 40 |  |  | 40 |  |
| Link Distance（ft） |  | 873 |  |  | 308 |  |  | 454 |  |  | 853 |  |
| Travel Time（s） |  | 14.9 |  |  | 5.3 |  |  | 7.7 |  |  | 14.5 |  |
| Confl．Peds．（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Confl．Bikes（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 | 0.98 |
| Growth Factor | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ | 100\％ |
| Heavy Vehicles（\％） | 2\％ | 1\％ | 3\％ | 2\％ | 2\％ | 5\％ | 3\％ | 3\％ | 2\％ | 2\％ | 3\％ | 0\％ |
| Bus Blockages（\＃／hr） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Parking（\＃／hr） |  |  |  |  |  |  |  |  |  |  |  |  |
| Mid－Block Traffic（\％） |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Shared Lane Traffic（\％） |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow（vph） | 113 | 322 | 347 | 123 | 812 | 343 | 433 | 1481 | 48 | 490 | 1477 | 67 |
| Turn Type | Prot | NA | pm＋ov | Prot | NA | pm＋ov | Prot | NA | pm＋ov | Prot | NA | pm＋ov |
| Protected Phases | 7 | 4 | 5 | 3 | 8 | 1 | 5 | 2 | 3 | 1 | 6 | 7 |
| Permitted Phases |  |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |
| Detector Phase | 7 | 4 | 5 | 3 | 8 | 1 | 5 | 2 | 3 | 1 | 6 | 7 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 3.0 | 8.0 | 4.0 | 3.0 | 8.0 | 4.0 | 4.0 | 15.0 | 3.0 | 4.0 | 15.0 | 3.0 |
| Minimum Split（s） | 7.5 | 24.0 | 8.5 | 7.5 | 24.0 | 8.5 | 8.5 | 24.0 | 7.5 | 8.5 | 43.0 | 7.5 |
| Total Split（s） | 14.0 | 32.0 | 22.0 | 14.0 | 32.0 | 21.0 | 22.0 | 53.0 | 14.0 | 21.0 | 52.0 | 14.0 |
| Total Split（\％） | 11．7\％ | 26．7\％ | 18．3\％ | 11．7\％ | 26．7\％ | 17．5\％ | 18．3\％ | 44．2\％ | 11．7\％ | 17．5\％ | 43．3\％ | 11．7\％ |
| Yellow Time（s） | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 | 3.5 | 3.5 | 4.5 | 3.5 |
| All－Red Time（s） | 1.0 | 1.5 | 1.0 | 1.0 | 1.5 | 1.0 | 1.0 | 1.5 | 1.0 | 1.0 | 1.5 | 1.0 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 4.5 | 6.0 | 4.5 | 4.5 | 6.0 | 4.5 | 4.5 | 6.0 | 4.5 | 4.5 | 6.0 | 4.5 |
| Lead／Lag | Lead | Lag | Lead | Lead | Lag | Lead | Lead | Lag | Lead | Lead | Lag | Lead |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | None | None | None | None | None | None | C－Min | None | None | C－Min | None |
| Act Effct Green（s） | 8.7 | 25.7 | 49.1 | 8.8 | 25.8 | 49.3 | 17.4 | 47.0 | 61.8 | 17.5 | 47.1 | 61.8 |
| Actuated g／C Ratio | 0.07 | 0.21 | 0.41 | 0.07 | 0.22 | 0.41 | 0.14 | 0.39 | 0.52 | 0.15 | 0.39 | 0.52 |


|  | * |  |  | $\checkmark$ |  |  | 4 | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| v/c Ratio | 0.47 | 0.41 | 0.53 | 0.50 | 0.73 | 0.53 | 0.91 | 1.03 | 0.06 | 1.01 | 1.06 | 0.08 |
| Control Delay | 59.9 | 42.5 | 24.3 | 60.8 | 48.2 | 24.6 | 74.5 | 66.8 | 1.8 | 95.4 | 76.4 | 3.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 59.9 | 42.5 | 24.3 | 60.8 | 48.2 | 24.6 | 74.5 | 66.8 | 1.8 | 95.4 | 76.4 | 3.7 |
| LOS | E | D | C | E | D | C | E | E | A | F | E | A |
| Approach Delay |  | 36.9 |  |  | 43.1 |  |  | 66.9 |  |  | 78.6 |  |
| Approach LOS |  | D |  |  | D |  |  | E |  |  | E |  |
| Queue Length 50th (ft) | 43 | 113 | 158 | 47 | 215 | 159 | 172 | $\sim 643$ | 0 | $\sim 217$ | $\sim 673$ | 0 |
| Queue Length 95th (ft) | 74 | 159 | 252 | 79 | 264 | 253 | \#264 | \#782 | 11 | \#325 | \#812 | 22 |
| Internal Link Dist (ft) |  | 793 |  |  | 228 |  |  | 374 |  |  | 773 |  |
| Turn Bay Length (ft) | 220 |  | 520 | 285 |  | 480 | 450 |  | 480 | 485 |  | 600 |
| Base Capacity (vph) | 262 | 793 | 661 | 262 | 1132 | 650 | 479 | 1444 | 857 | 484 | 1398 | 846 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.43 | 0.41 | 0.52 | 0.47 | 0.72 | 0.53 | 0.90 | 1.03 | 0.06 | 1.01 | 1.06 | 0.08 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Area Type: Other |  |  |  |  |  |  |  |  |  |  |  |  |
| Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length: 120 |  |  |  |  |  |  |  |  |  |  |  |  |
| Offset: 33 (28\%), Referenced to phase 2:NBT and 6:SBT, Start of Green |  |  |  |  |  |  |  |  |  |  |  |  |
| Natural Cycle: 95 |  |  |  |  |  |  |  |  |  |  |  |  |
| Control Type: Actuated-Coordinated |  |  |  |  |  |  |  |  |  |  |  |  |
| Maximum v/c Ratio: 1.06 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Signal Delay: 61.9 |  |  |  |  | Intersection LOS: E |  |  |  |  |  |  |  |
| Intersection Capacity Utilization 87.2\% ICU Level of Service E |  |  |  |  |  |  |  |  |  |  |  |  |
| Analysis Period (min) 15 |  |  |  |  |  |  |  |  |  |  |  |  |
| ~ Volume exceeds capacity, queue is theoretically infinite. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maximum after two cycles. |  |  |  |  |  |  |  |  |  |  |  |  |

Splits and Phases: 1: Milwaukee Avenue \& Deerfield Road




HCM 6th TWSC
3: Cubesmart Access Road/West Site Access Drive \& Deerfield Road




| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :---: | :---: | :---: | :---: | :---: | ---: | ---: |
| Conflicting Flow All | - | 0 | - | 0 | - | 635 |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |
| Critical Hdwy | - | - | - | - | - | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | - | - |
| Critical Hdwy Stg 2 | - | - | - | - | - | - |
| Follow-up Hdwy | - | - | - | - | - | 3.3 |
| Pot Cap-1 Maneuver | 0 | - | - | 0 | 0 | 426 |
| $\quad$ Stage 1 | 0 | - | - | 0 | 0 | - |
| Stage 2 | 0 | - | - | 0 | 0 | - |
| Platoon blocked, \% |  | - | - |  |  |  |
| Mov Cap-1 Maneuver | - | - | - | - | - | 426 |
| Mov Cap-2 Maneuver | - | - | - | - | - | - |
| Stage 1 | - | - | - | - | - | - |
| Stage 2 | - | - | - | - | - | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 13.6 |
| HCM LOS |  | $B$ |  |


| Minor Lane/Major Mvmt | EBT | WBT SBLn1 |
| :--- | :---: | ---: |
| Capacity (veh/h) | - | -426 |
| HCM Lane V/C Ratio | - | -0.012 |
| HCM Control Delay (s) | - | -13.6 |
| HCM Lane LOS | - | - |
| HCM 95th \%tile Q(veh) | - | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.2 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | i | 个 | 个 |  |  |  |
| Traffic Vol, veh/h | 5 | 794 | 1205 | 12 | 4 |  |
| Future Vol, veh/h | 5 | 794 | 1205 | 12 | 4 | 5 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 50 | - | - | - | 0 | - |
| Veh in Median Storage, \# | - | 0 | 0 | - | 1 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 82 | 82 | 82 | 82 | 82 | 82 |
| Heavy Vehicles, $\%$ | 0 | 2 | 3 | 0 | 0 | 0 |
| Mvmt Flow | 6 | 968 | 1470 | 15 | 5 | 6 |


| Major/Minor M | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 1485 | 0 | - | 0 | 2458 | 743 |
| Stage 1 | - | - | - | - | 1478 | - |
| Stage 2 | - | - | - | - | 980 | - |
| Critical Hdwy | 4.1 | - | - | - | 6.6 | 6.9 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.8 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.4 | - |
| Follow-up Hdwy | 2.2 | - | - | - | 3.5 | 3.3 |
| Pot Cap-1 Maneuver | 459 | - | - | - | 30 | 362 |
| Stage 1 | - | - | - | - | 179 | - |
| Stage 2 | - | - | - | - | 367 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 459 | - | - | - | 30 | 362 |
| Mov Cap-2 Maneuver | - | - | - | - | 121 | - |
| Stage 1 | - | - | - | - | 177 | - |
| Stage 2 | - | - | - | - | 367 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.1 |  | 0 |  | 24.9 |  |
| HCM LOS |  |  |  |  | C |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT | WBR SBLn1 |  |
| Capacity (veh/h) |  | 459 | - | - | - | 192 |
| HCM Lane V/C Ratio |  | 0.013 | - | - | - | 0.057 |
| HCM Control Delay (s) |  | 12.9 | - | - | - | 24.9 |
| HCM Lane LOS |  | B | - | - | - | C |
| HCM 95th \%tile Q(veh) |  | 0 | - | - | - | 0.2 |


[^0]:    ${ }^{1}$ IDOT DISCLAIMER: The motor vehicle crash data referenced herein was provided by the Illinois Department of Transportation. Any conclusions drawn from analysis of the aforementioned data are the sole responsibility of the data recipient(s). Additionally, for coding years 2015 to present, the Bureau of Data Collection uses the exact latitude/longitude supplied by the investigating law enforcement agency to locate crashes. Therefore, location data may vary in previous years since data prior to 2015 was physically located by bureau personnel.

